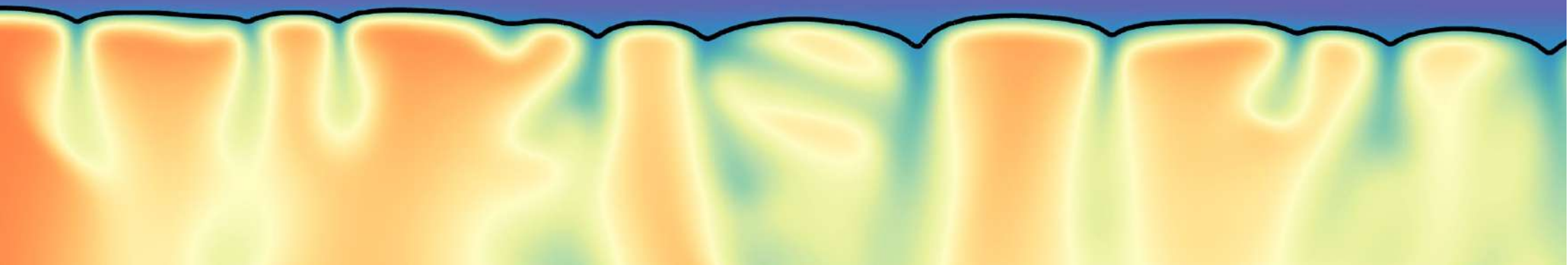


# Numerical simulations of convective mixing with complex fluids



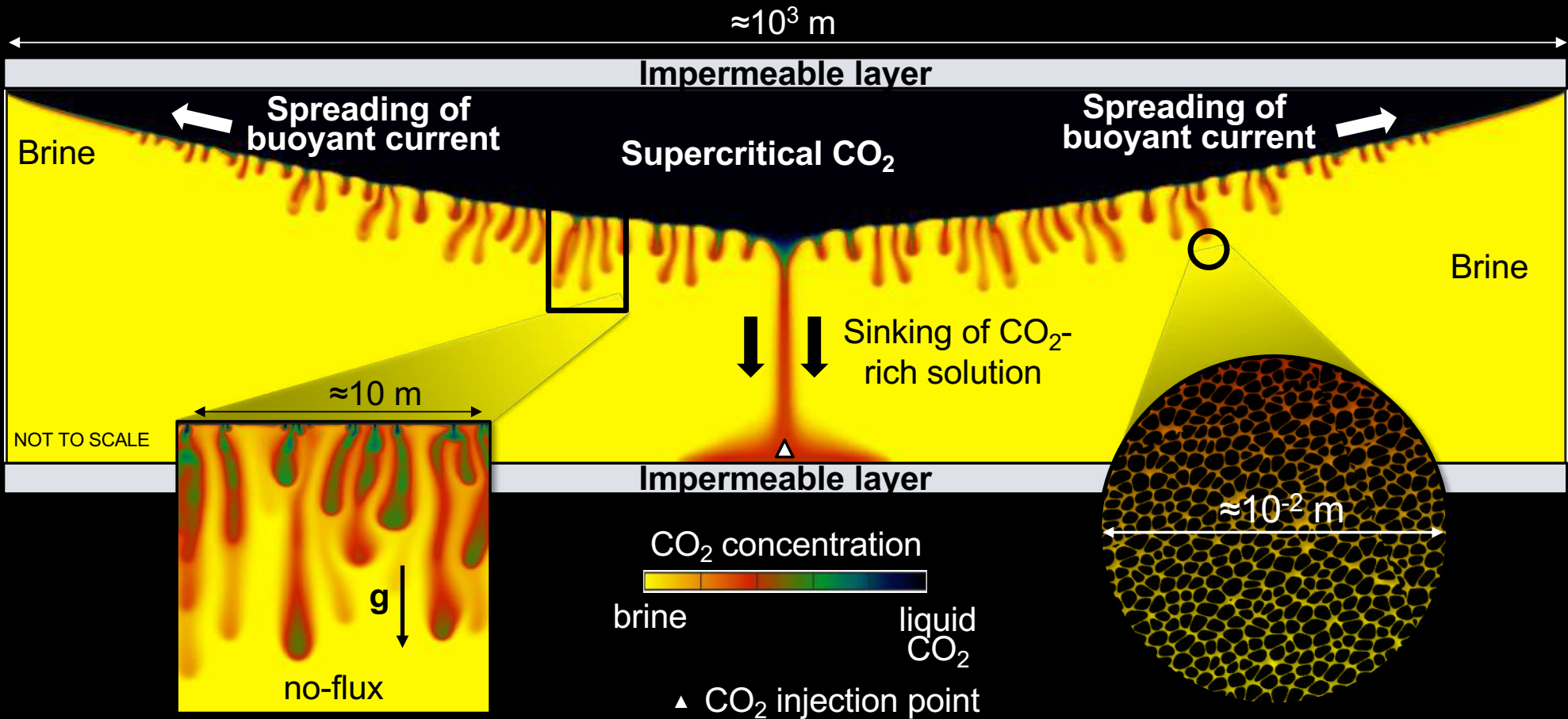
**Marco De Paoli<sup>1</sup> & Sergio Pirozzoli<sup>2</sup>**

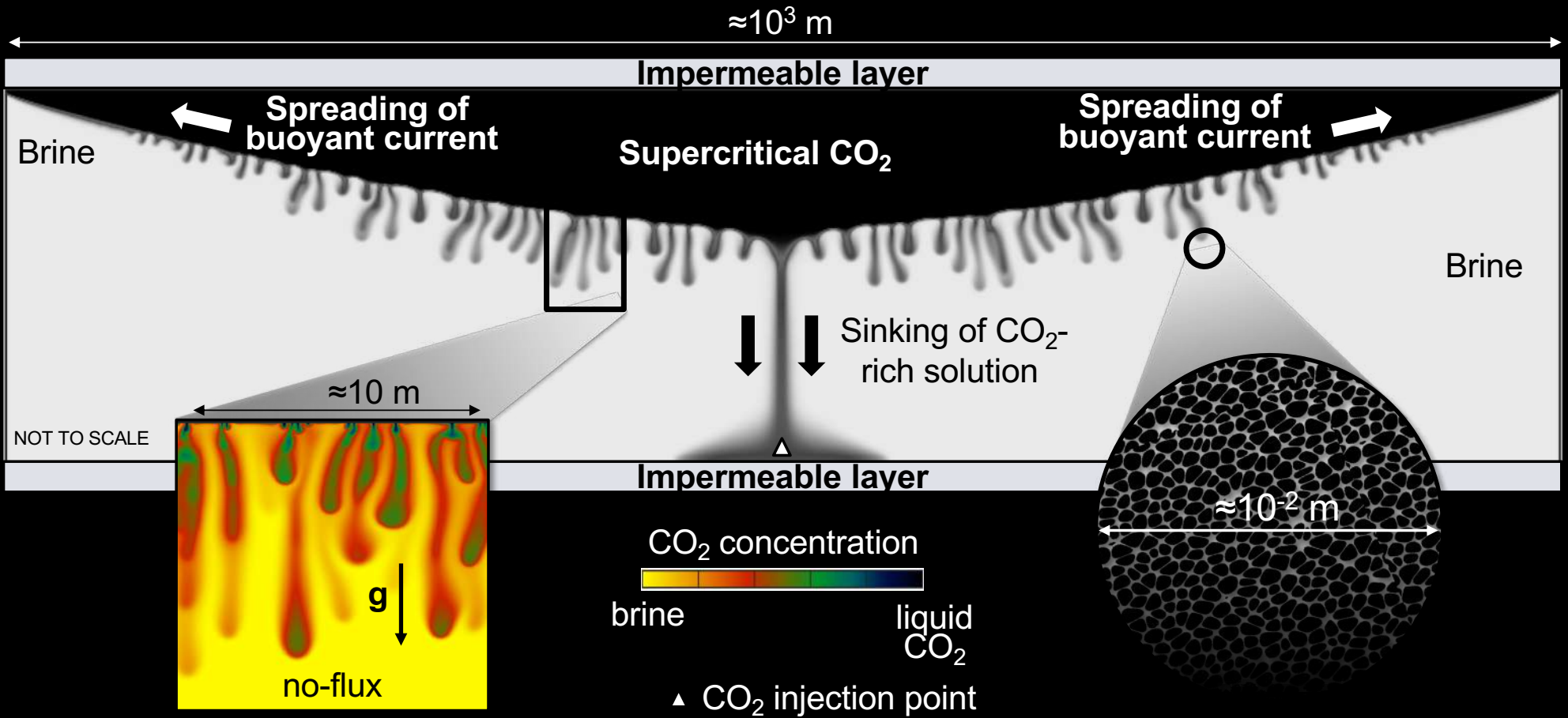
<sup>1</sup>TU Wien, Vienna, Austria

<sup>2</sup>Sapienza University, Rome, Italy

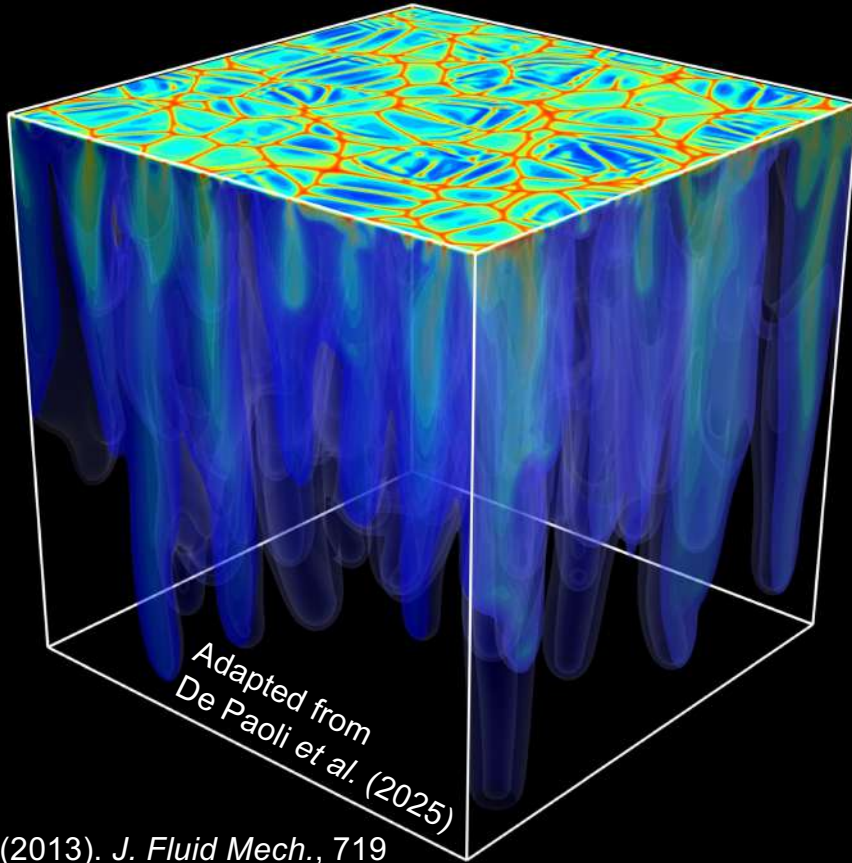
[marco.de.paoli@tuwien.ac.at](mailto:marco.de.paoli@tuwien.ac.at)







Fixed interface



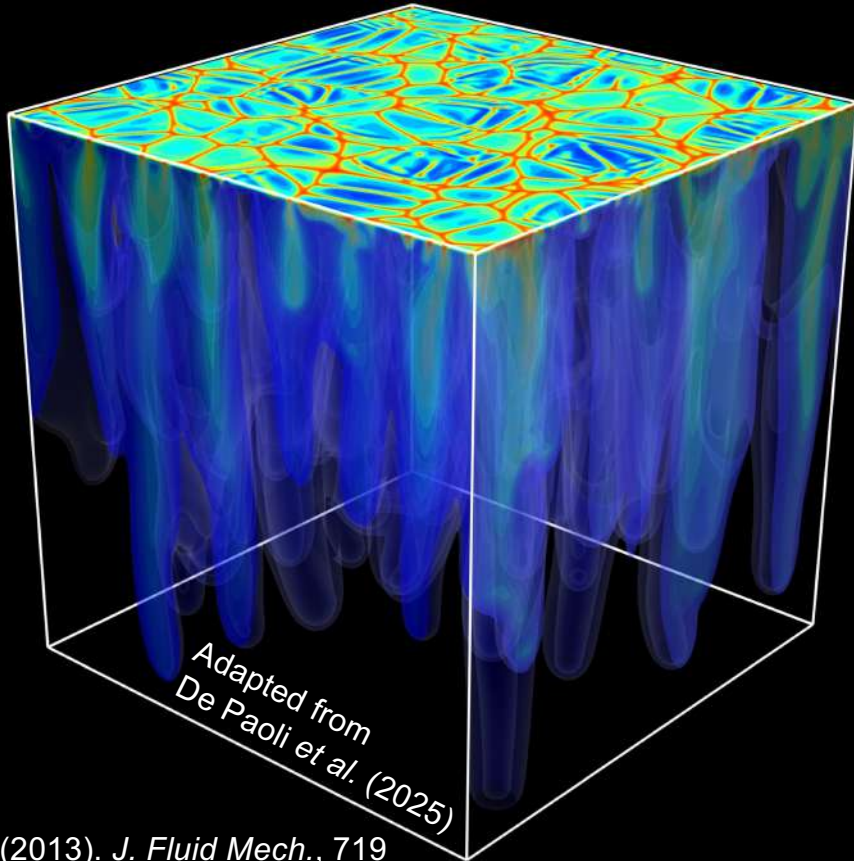
Adapted from  
De Paoli et al. (2025)

Hewitt et al. (2013). *J. Fluid Mech.*, 719

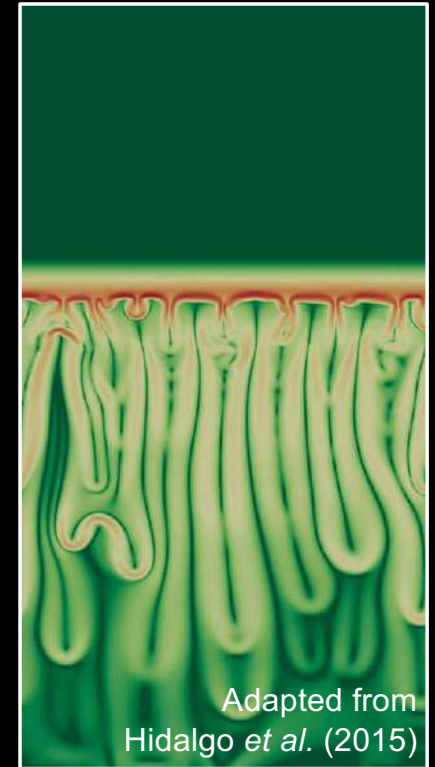
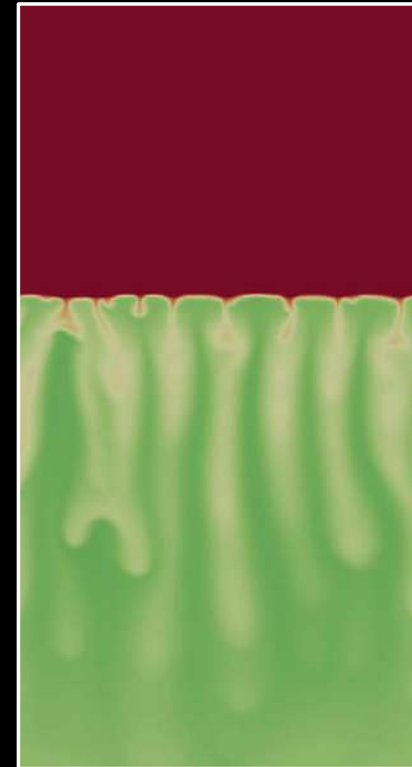
Slim, A. (2014). *J. Fluid Mech.*, 741

De Paoli et al. (2025). *Geophys. Res. Lett.*, 52 (7)

Fixed interface



Free interface



Hewitt et al. (2013). *J. Fluid Mech.*, 719

Slim, A. (2014). *J. Fluid Mech.*, 741

De Paoli et al. (2025). *Geophys. Res. Lett.*, 52 (7)

Hewitt et al. (2013). *J. Fluid Mech.*, 719

Hidalgo et al. (2015). *Geophys. Res. Lett.*, 42 (15)

Imuetinyan et al. (2026). *The Eur. Phys. J. E*, 49 (20)

What is the role of boundary conditions?

What is the role of boundary conditions?

What is the role of fluid model?

What is the role of boundary conditions?

What is the role of fluid model?

What is the role of dimensionality?

Flow

$$\nabla \cdot \mathbf{u} = 0$$

$$\mathbf{u} = -(\nabla p + \rho \mathbf{k})$$

$$\frac{\partial C}{\partial t} + \mathbf{u} \cdot \nabla C = \frac{1}{Ra_0} \nabla^2 C$$

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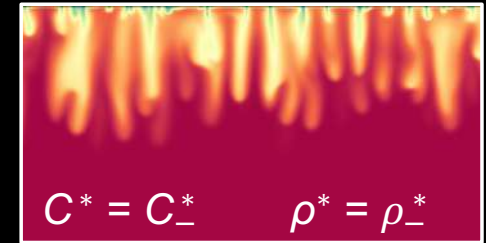
Fluid

Fixed interface

$$\rho = 1 + C, \quad -1 \leq C \leq 0$$

$$\rho = 1 - C^2, \quad -1 \leq C \leq 0$$

$$C^* = C_m^*, \quad \rho^* = \rho_m^* \quad z^* = H^*$$



$$C^* = C_-^*, \quad \rho^* = \rho_-^* \quad z^* = 0$$

Flow

$$\nabla \cdot \mathbf{u} = 0$$

$$\mathbf{u} = -(\nabla p + \rho \mathbf{k})$$

$$\frac{\partial C}{\partial t} + \mathbf{u} \cdot \nabla C = \frac{1}{Ra_0} \nabla^2 C$$

Fluid

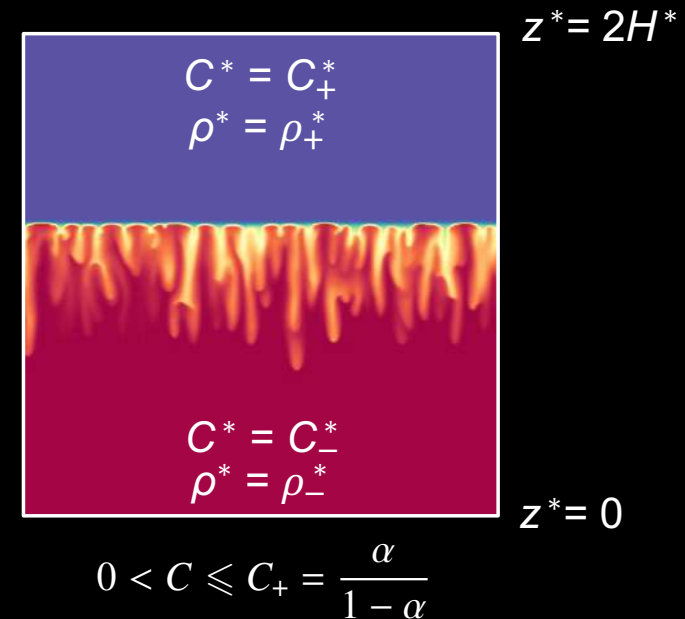
Fixed interface

$$\rho = 1 + C, \quad -1 \leq C \leq 0$$

$$\rho = 1 - C^2, \quad -1 \leq C \leq 0$$

Free interface

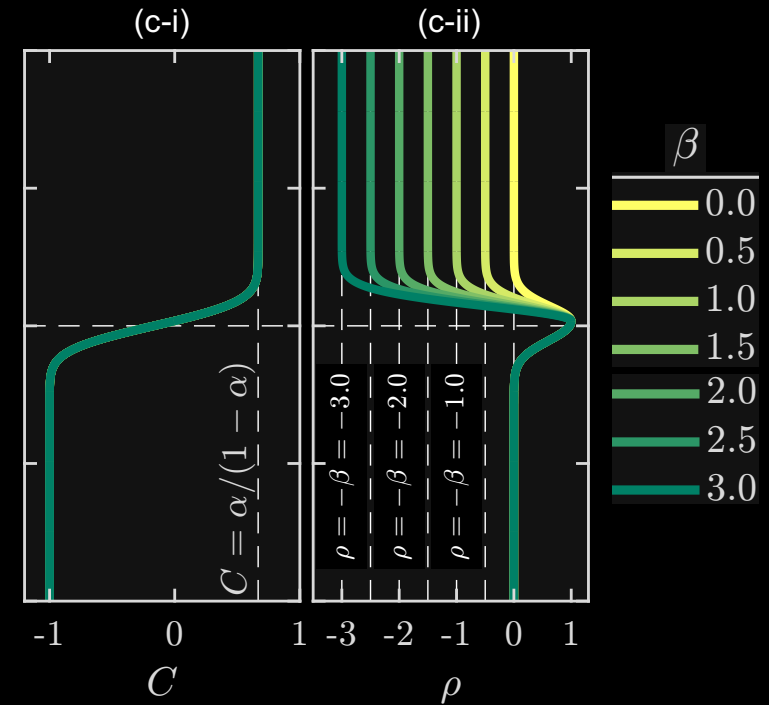
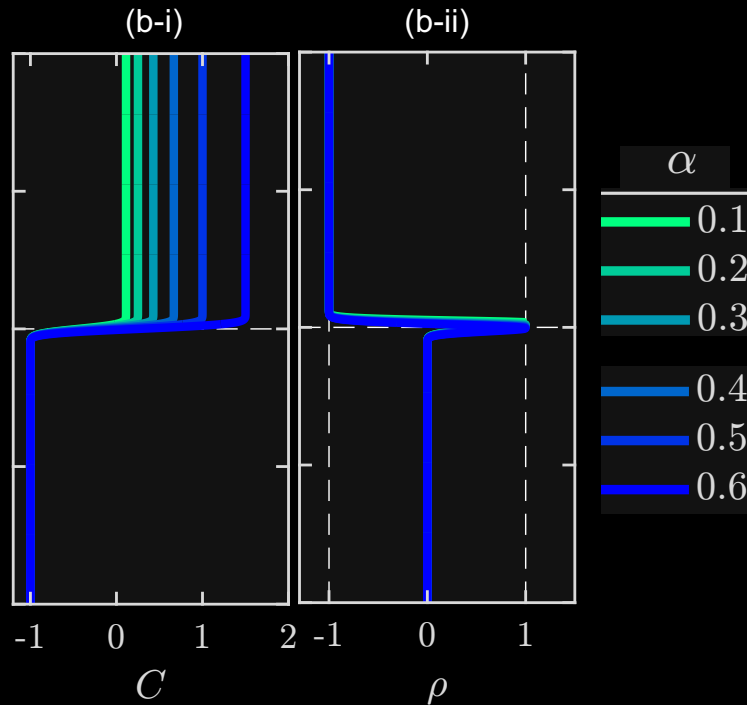
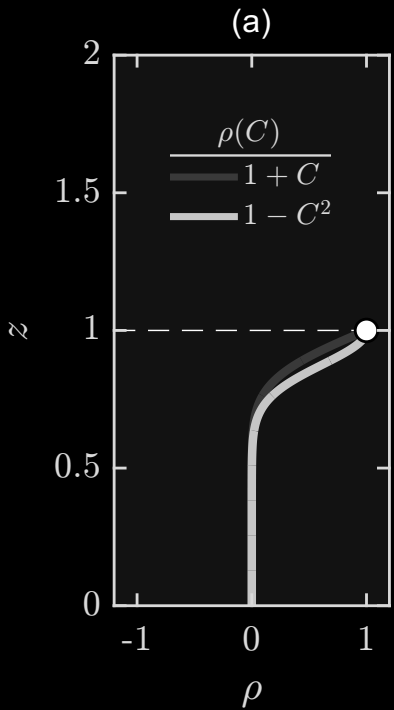
$$\rho = \begin{cases} 1 - C^2, & -1 \leq C \leq 0 \\ 1 - (1 + \beta) \left(1 - \frac{1}{\alpha}\right)^2 C^2, & 0 < C \leq C_+ \end{cases}$$



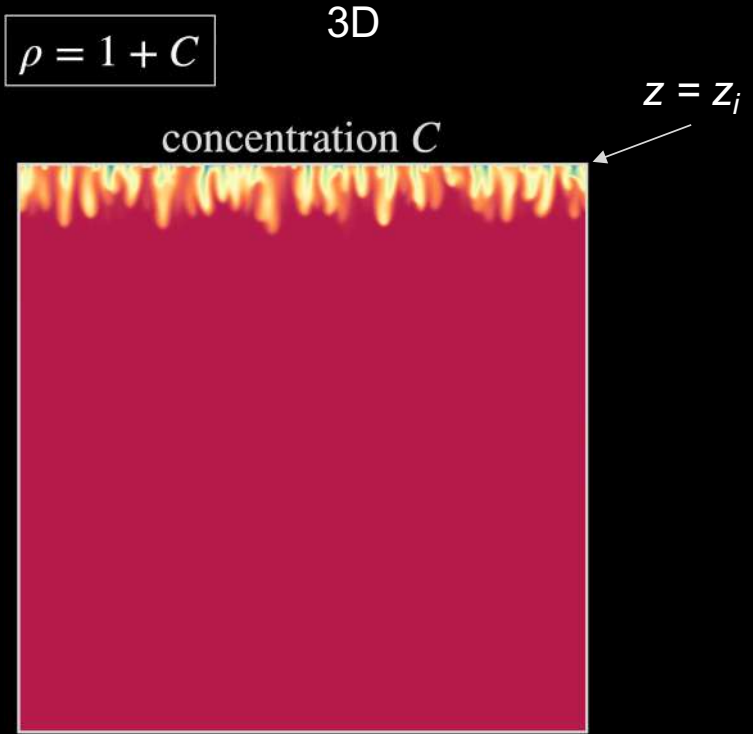
$$Ra_0 = \frac{\mathcal{U}^* H^*}{\phi D}, \quad \alpha = \frac{C_+^* - C_m^*}{C_+^* - C_-^*}, \quad \beta = \frac{\rho_-^* - \rho_+^*}{\rho_m^* - \rho_-^*}$$

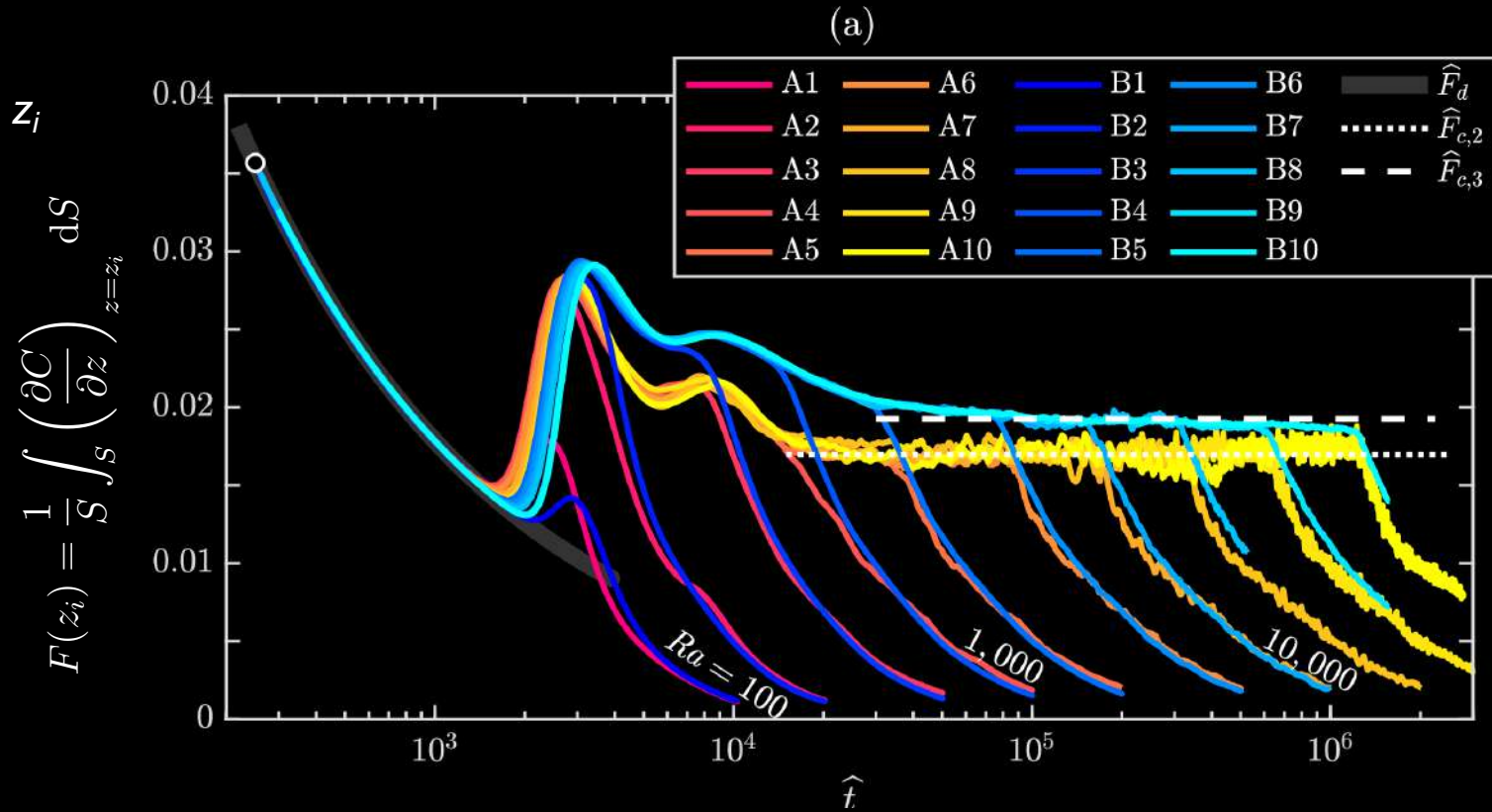
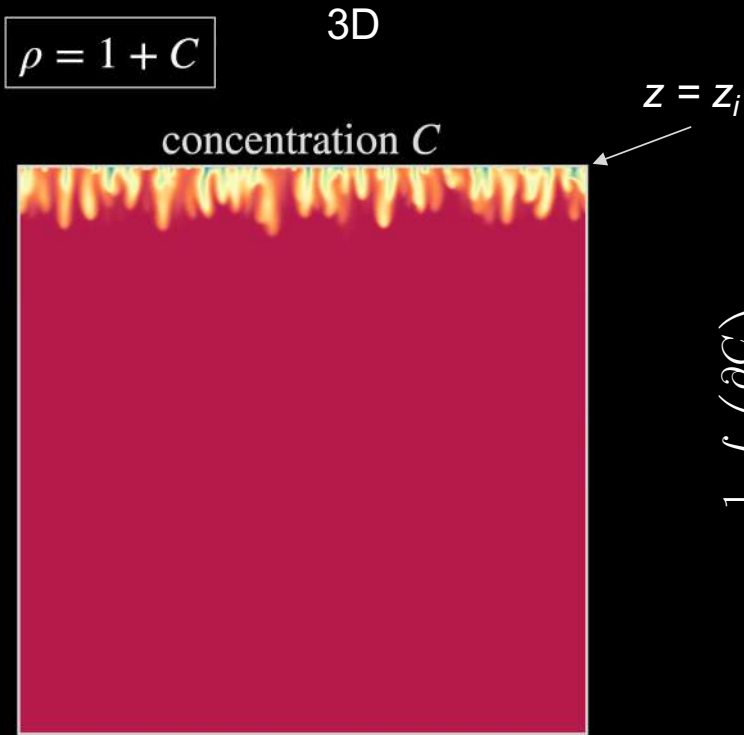
fixed interface

free interface

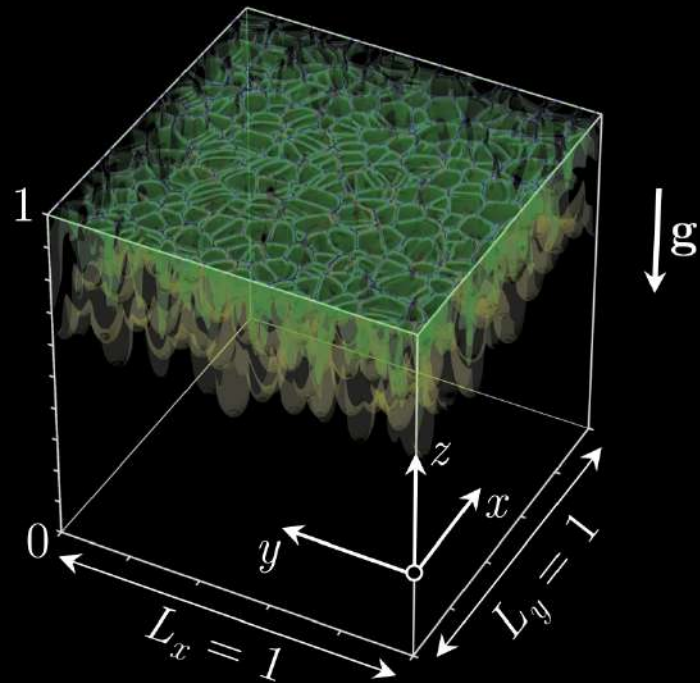


$$\alpha = \frac{C_+^* - C_m^*}{C_+^* - C_-^*}, \quad \beta = \frac{\rho_-^* - \rho_+^*}{\rho_m^* - \rho_-^*}$$

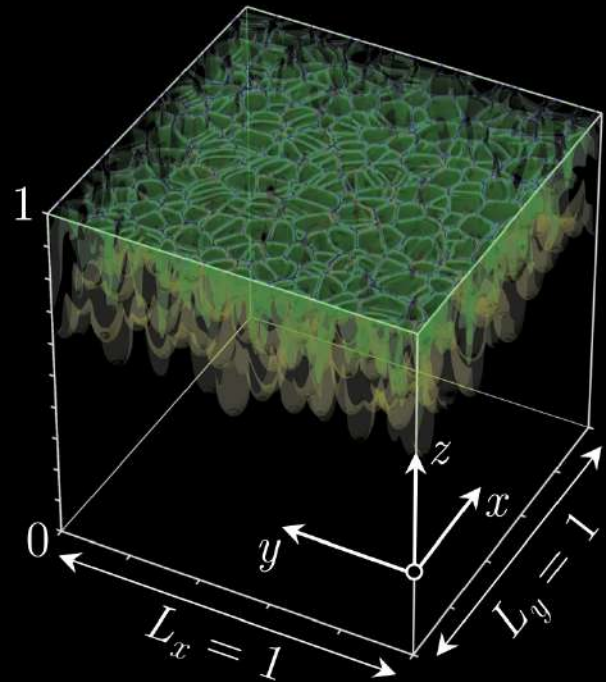




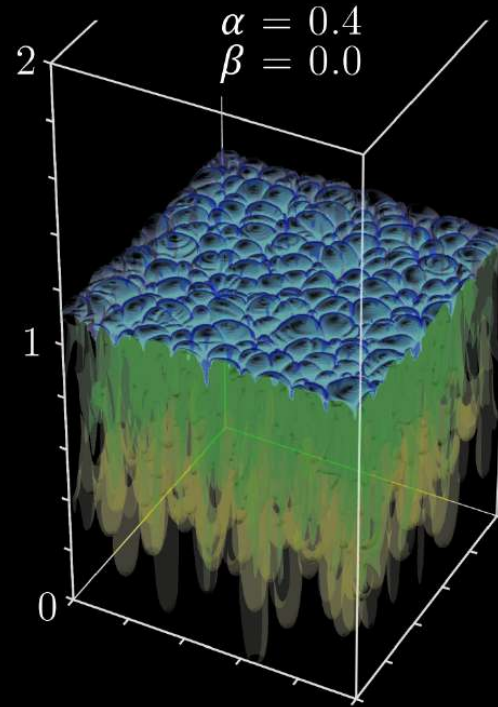
fixed interface  
(linear)



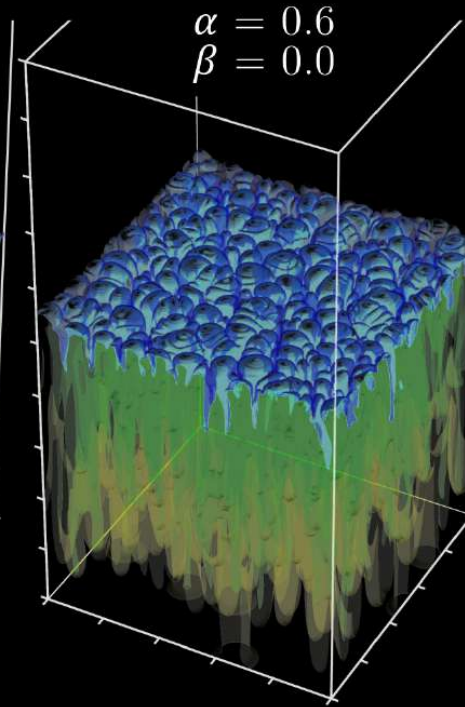
fixed interface  
(linear)



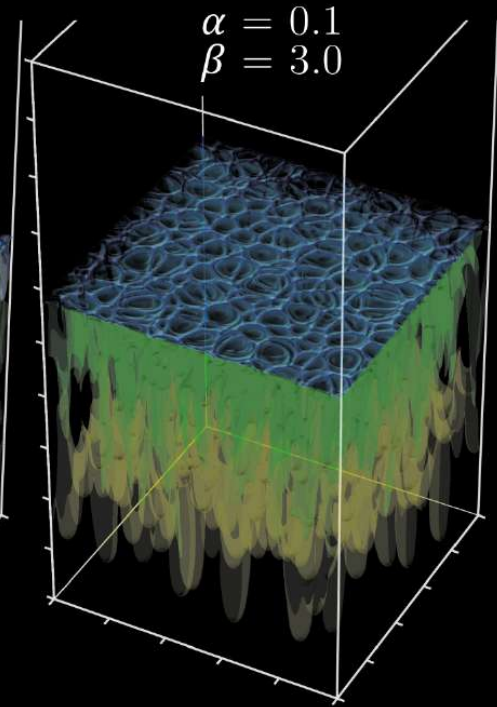
free interface



deformed interface



deformed interface

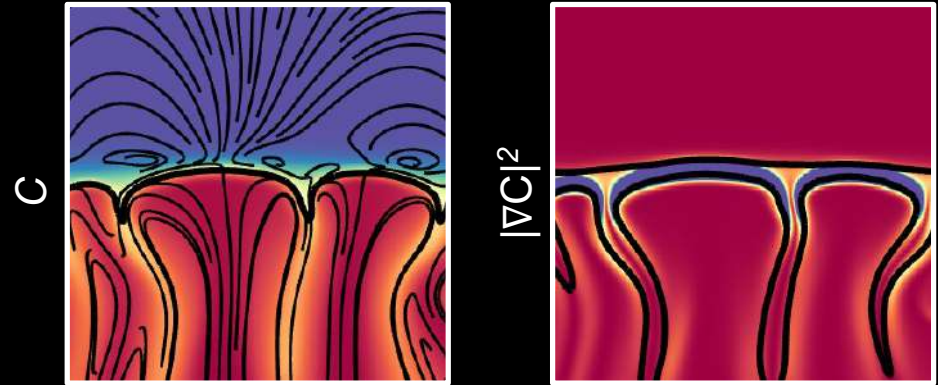


flat interface

Mean scalar dissipation

$$\chi = \langle |\nabla C|^2 \rangle$$

with  $\langle \quad \rangle$  = volume average

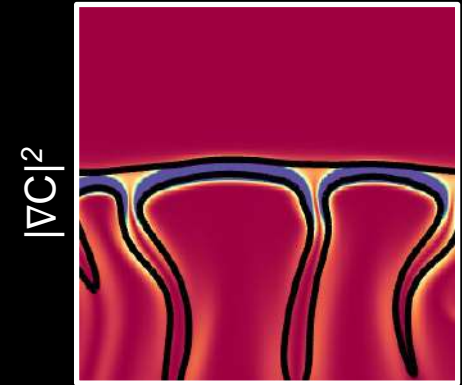
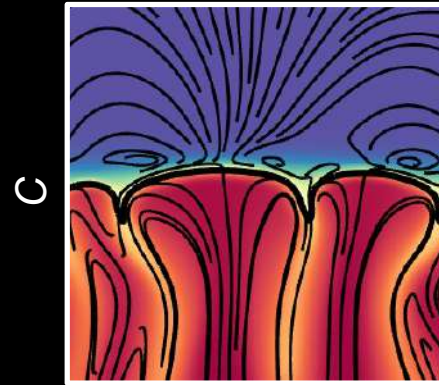


- Jha, B., Cueto-Felgueroso, L., & Juanes, R. (2011). *Phys. Rev. E*, 84 (6), 066312  
Hidalgo, J., Fe, J., Cueto-Felgueroso, L., & Juanes, R. (2012). *Phys. Rev. Lett.*, 109 (26), 264503.  
Hidalgo, J., Dentz, M., Cabeza, Y., & Carrera, J. (2015). *Geophys. Res. Lett.*, 42 (15), 6357–6364.

## Mean scalar dissipation

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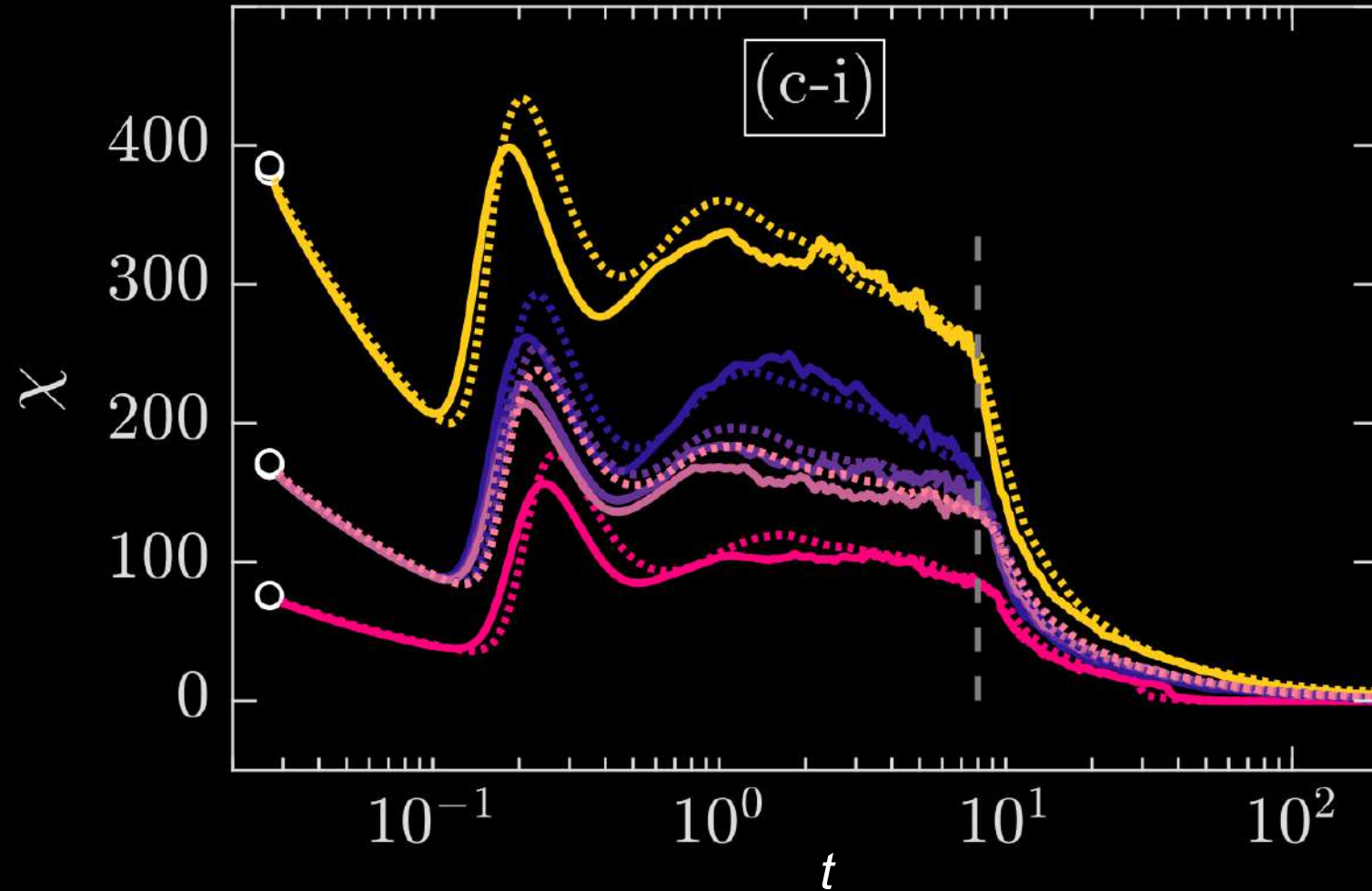
## Degree of mixing

$$M(t) = 1 - \frac{\sigma^2(t)}{\sigma_{\max}^2} = \frac{8(1 - \alpha)^2}{Ra} \int_0^t \chi dt$$

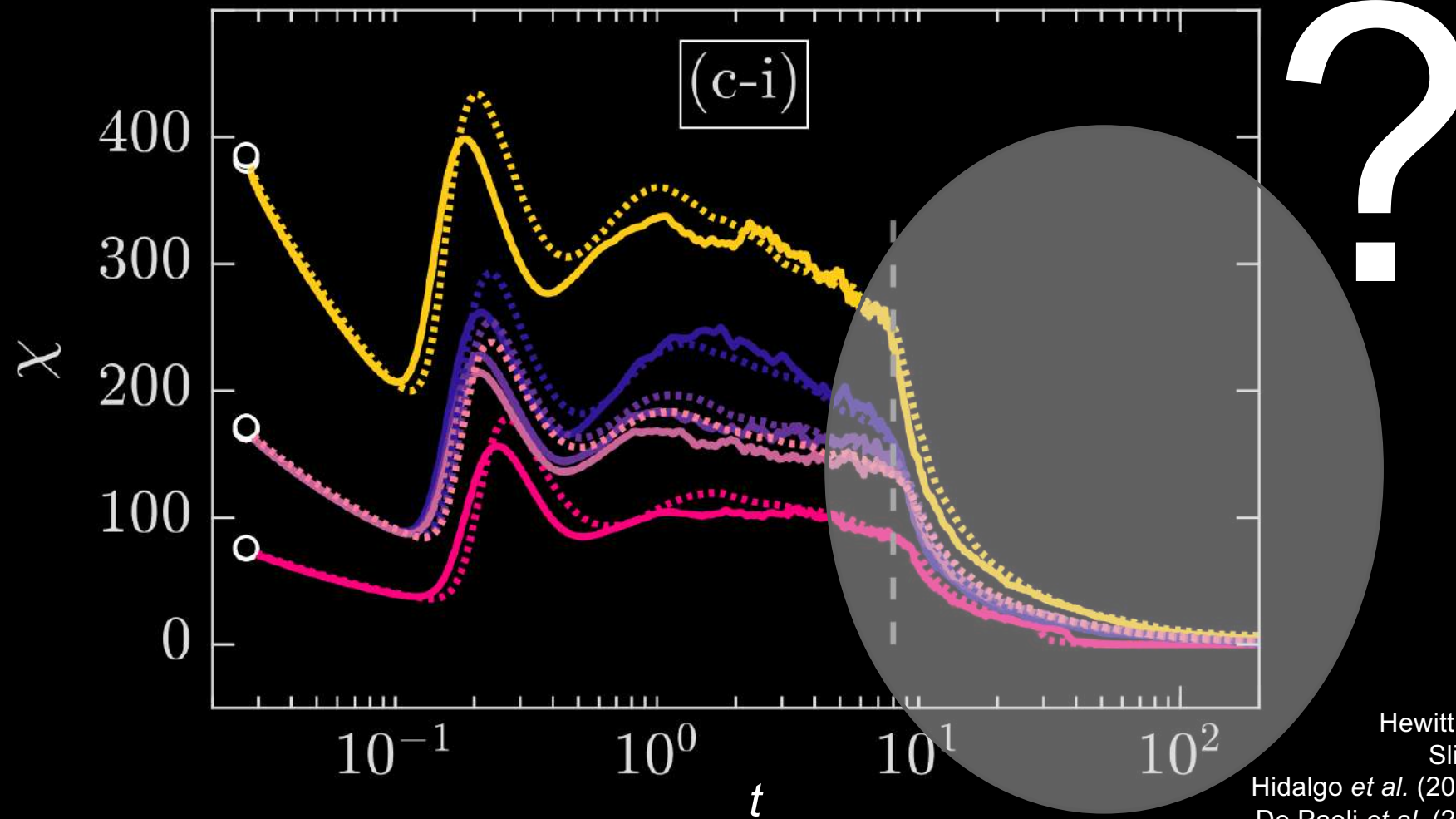
$$\sigma^2 = \langle C^2 \rangle - \langle C \rangle^2$$



- Jha, B., Cueto-Felgueroso, L., & Juanes, R. (2011). *Phys. Rev. E*, 84 (6), 066312  
 Hidalgo, J., Fe, J., Cueto-Felgueroso, L., & Juanes, R. (2012). *Phys. Rev. Lett.*, 109 (26), 264503.  
 Hidalgo, J., Dentz, M., Cabeza, Y., & Carrera, J. (2015). *Geophys. Res. Lett.*, 42 (15), 6357–6364.

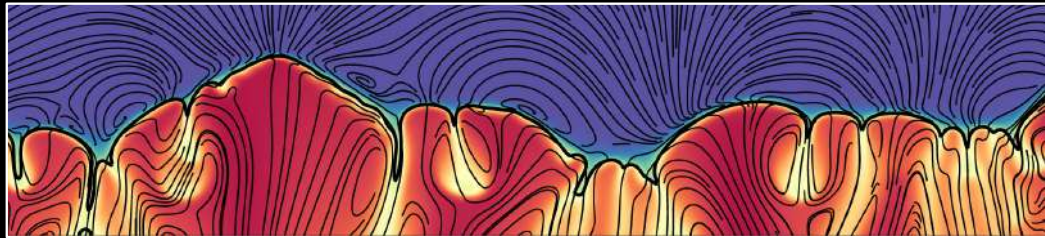


$$\chi = \langle |\nabla C|^2 \rangle$$

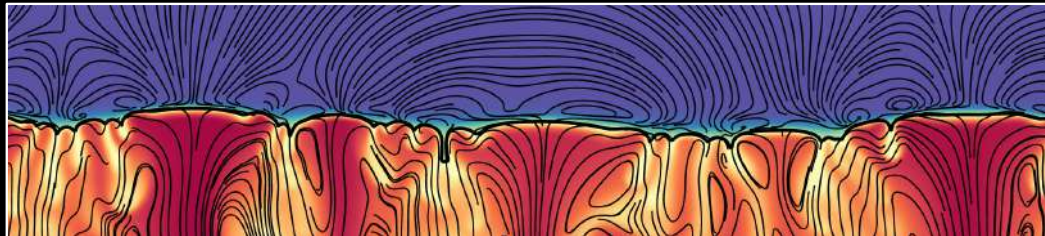


Hewitt et al. (2013). *J. Fluid Mech.*, 719  
 Slim, A. (2014). *J. Fluid Mech.*, 741  
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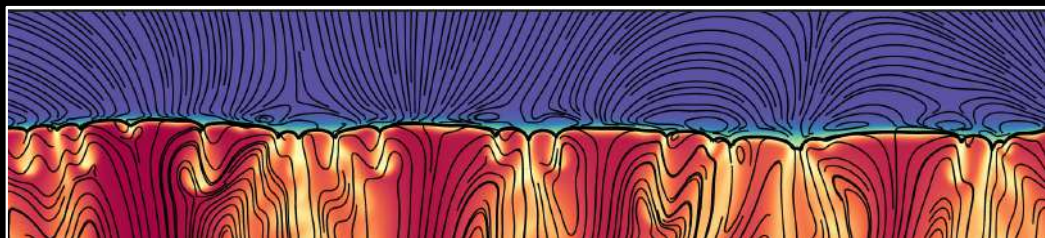
$\alpha = 0.4, \beta = 0.0$



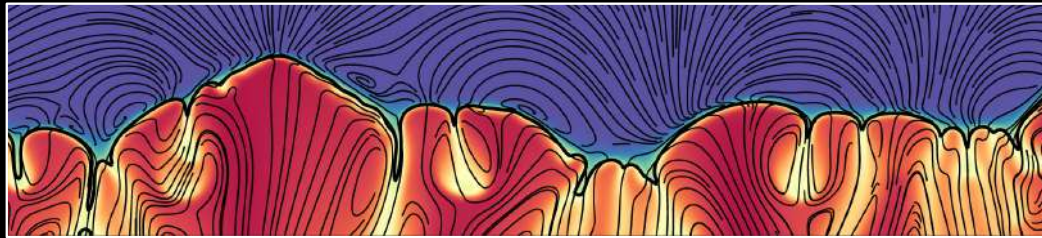
$\alpha = 0.4, \beta = 1.5$



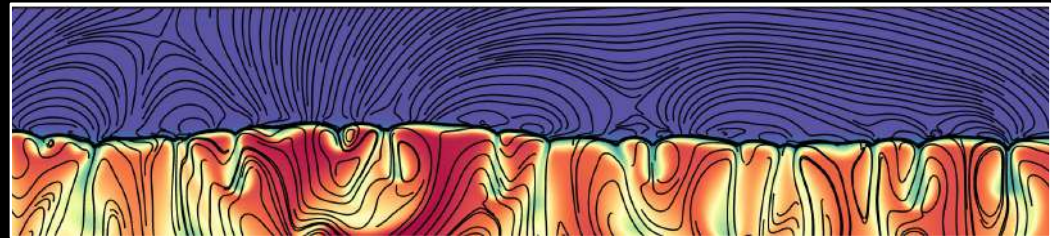
$\alpha = 0.4, \beta = 3.0$



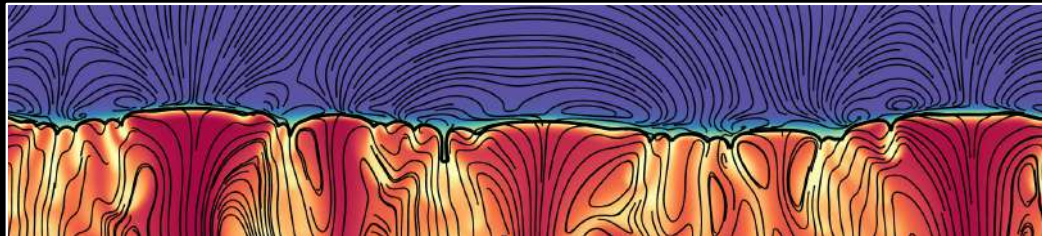
$\alpha = 0.4, \beta = 0.0$



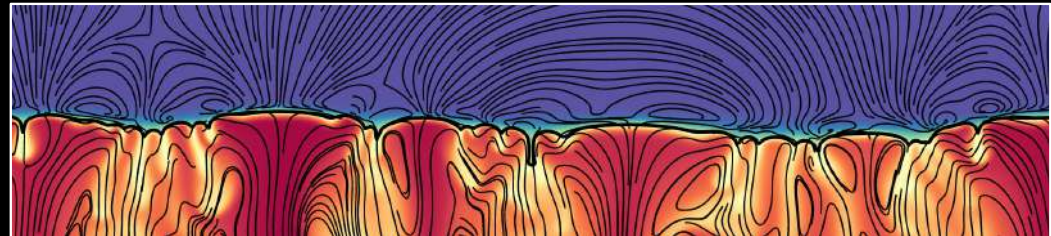
$\alpha = 0.1, \beta = 1.5$



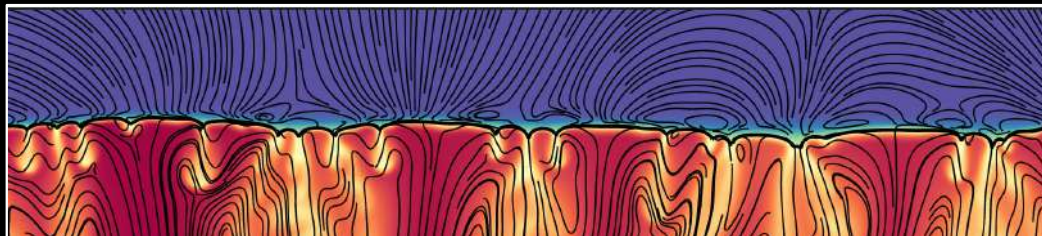
$\alpha = 0.4, \beta = 1.5$



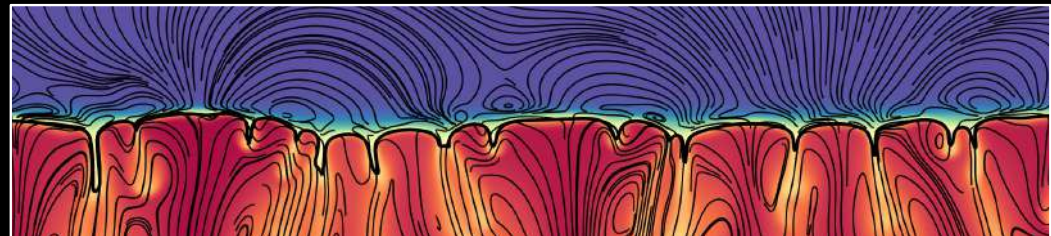
$\alpha = 0.4, \beta = 1.5$



$\alpha = 0.4, \beta = 3.0$



$\alpha = 0.6, \beta = 1.5$

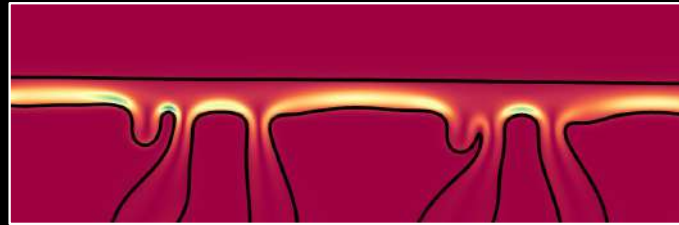


## Model for dissipation during shutdown of convection

$$\chi = \langle |\nabla C|^2 \rangle$$

1. Estimate local dissipation  $|\nabla C|^2$

$$|\partial_x C| \approx |\partial_y C| \ll |\partial_z C|$$



low  high

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low  high

2. Estimate boundary layer thickness

$$\delta(t) = (C_+ - C_-) f(t) = \frac{f(t)}{1 - \alpha}$$

$$C_+ - C_- = 1/(1 - \alpha)$$

$$f(t) = [a_1 + (t - t_s)]/a_2$$

**Interface deformation model**  
by Hidalgo et al. (2015)

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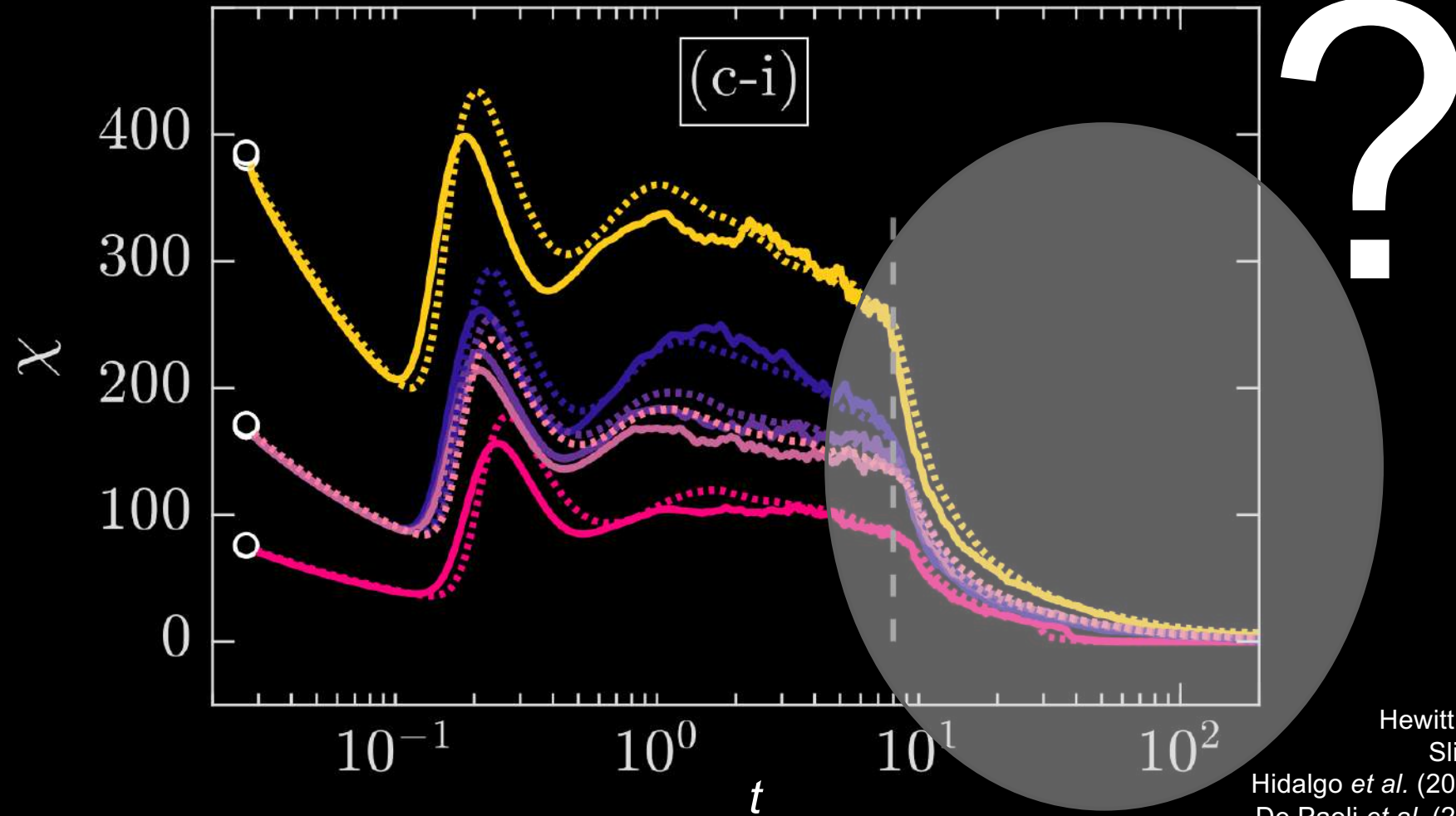
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**Interface deformation model**  
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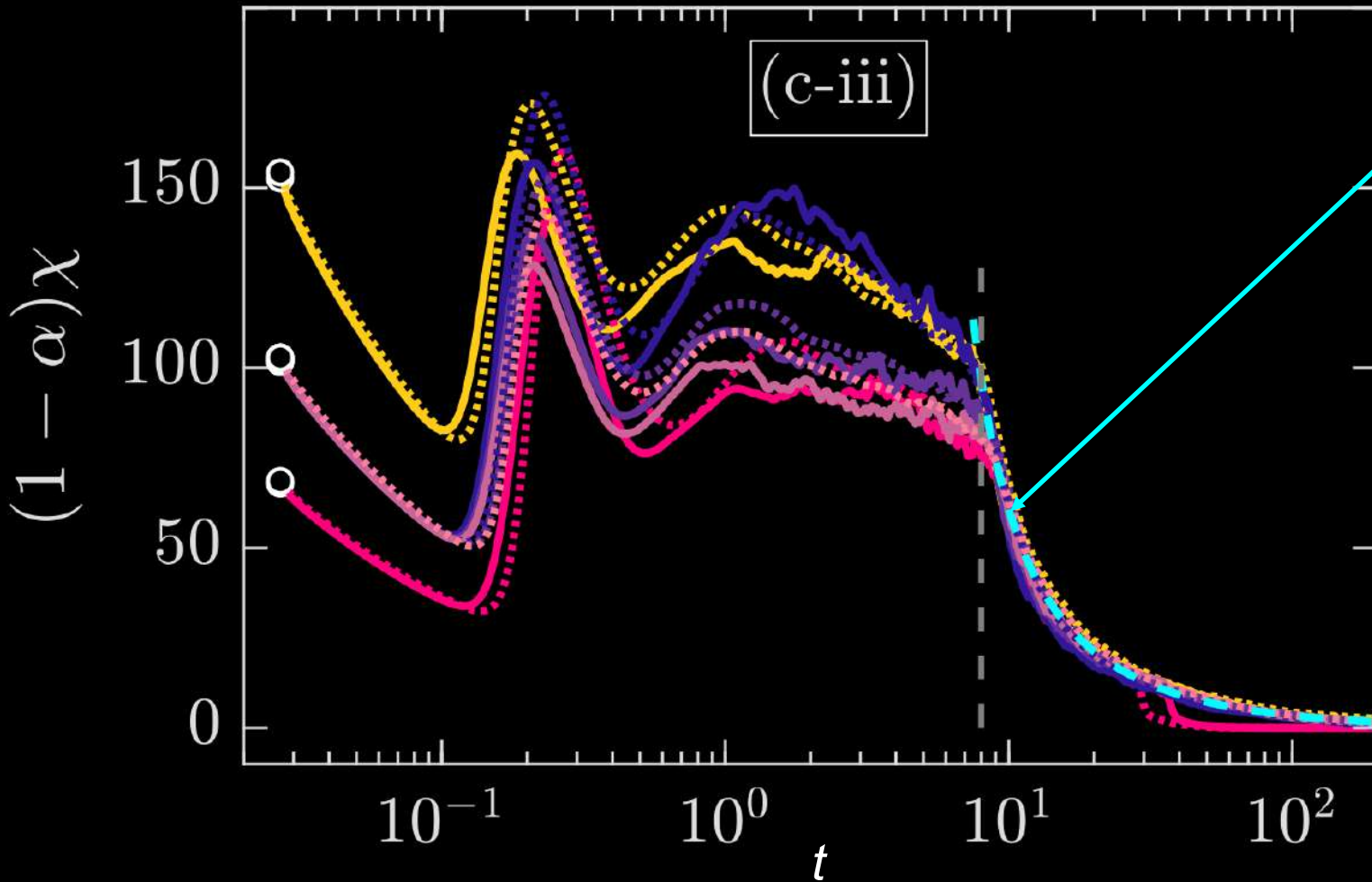
3. Combine and find dissipation

$$\chi = \langle |\nabla C|^2 \rangle \approx \frac{\delta}{L_z} \left( \frac{C_+ - C_-}{\delta} \right)^2$$

$$\chi_{sd}(t) = \frac{1}{2(1 - \alpha) f(t)}$$



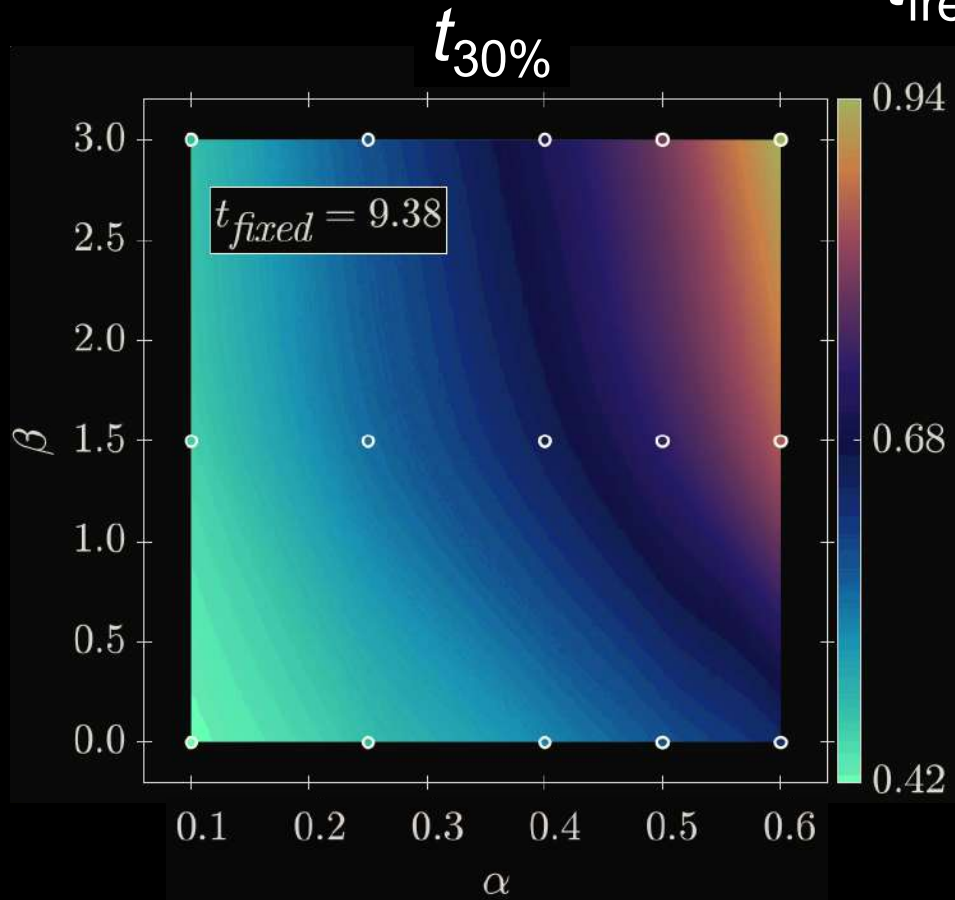
Hewitt et al. (2013). *J. Fluid Mech.*, 719  
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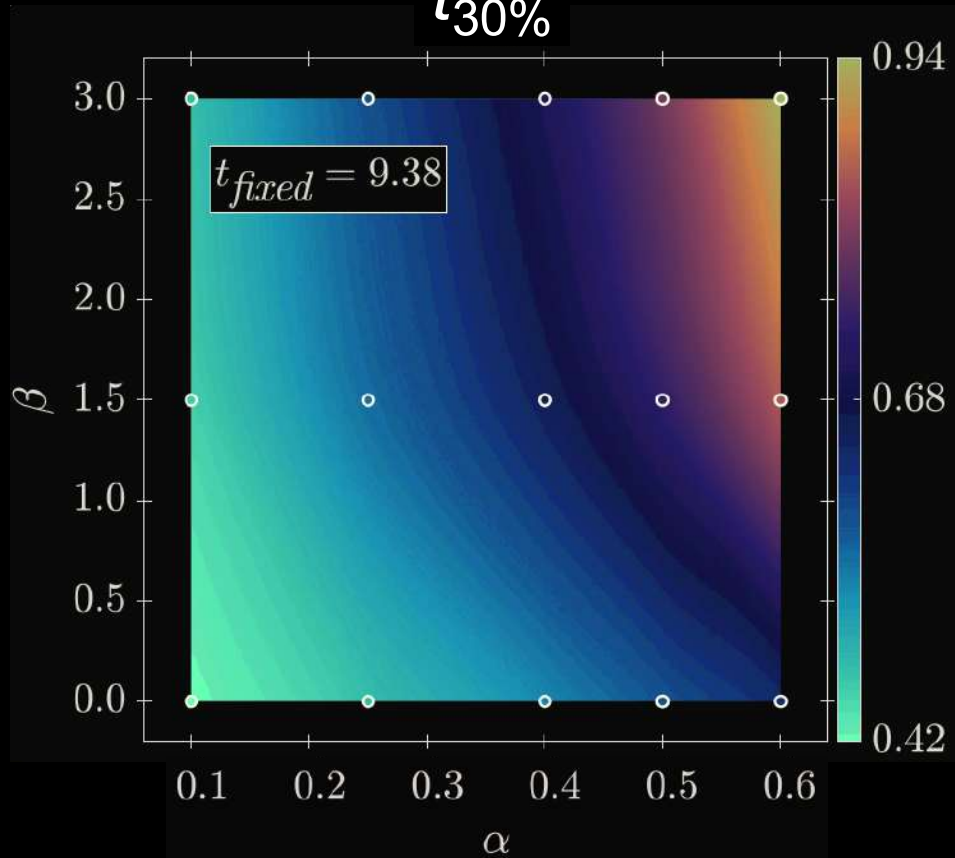
$$f(t) = [a_1 + (t - t_s)]/a_2$$

$t_{\text{free}} / t_{\text{fixed}}$  (3D, linear)

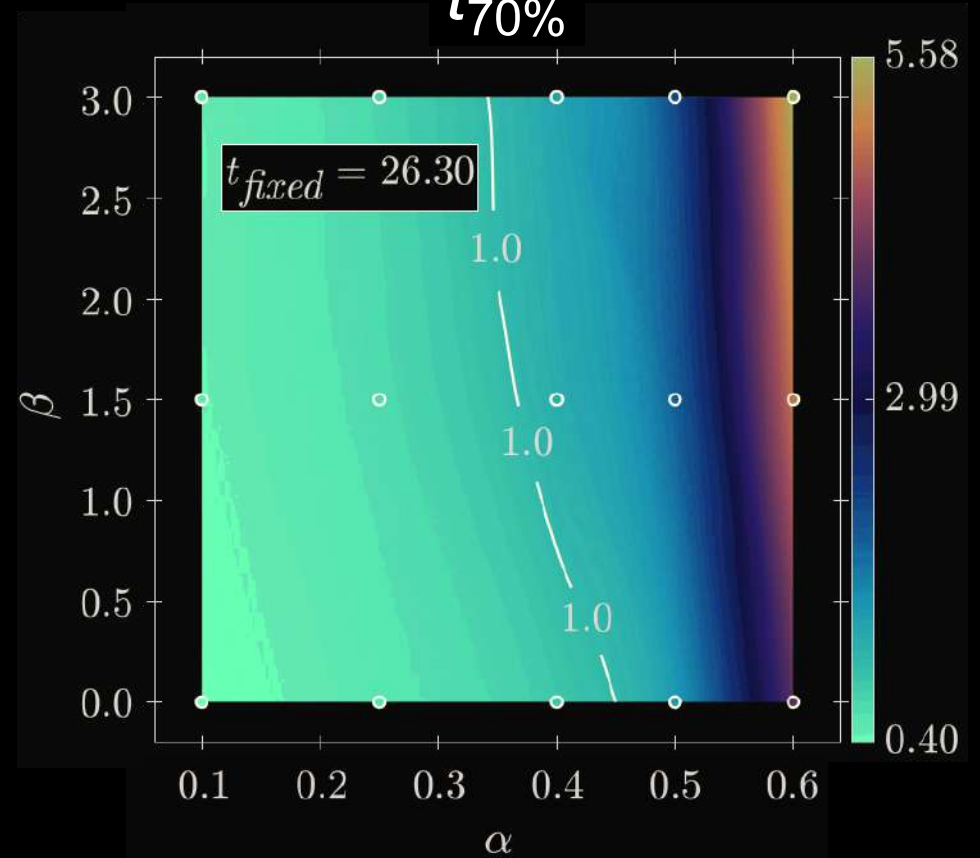


$t_{\text{free}} / t_{\text{fixed}}$  (3D, linear)

$t_{30\%}$



$t_{70\%}$



Theoretical framework for comparison of system with different b.c. and fluid models

De Paoli & Pirozzoli  
(arXiv:2604.23199)

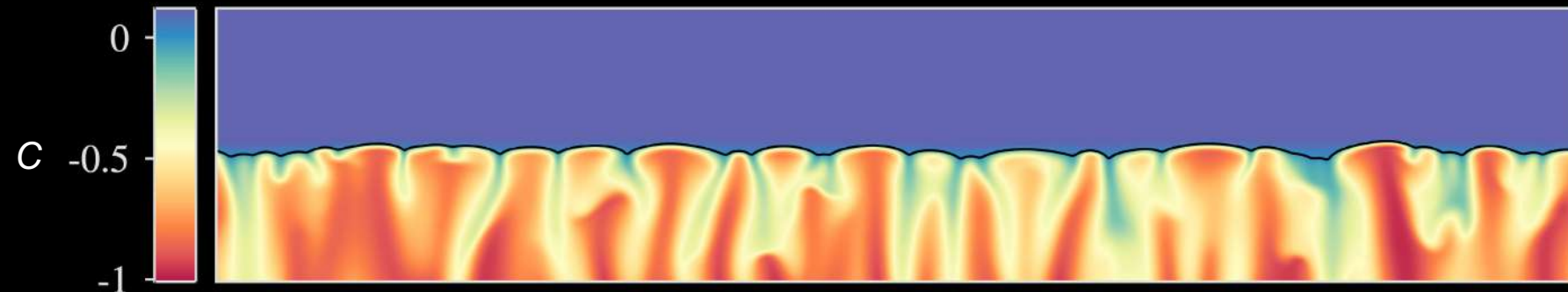


preprint



data

$\alpha = 0.1$   
 $\beta = 1.5$



Theoretical framework for comparison of system with different b.c. and fluid models

Understanding and modelling of mixing dynamics

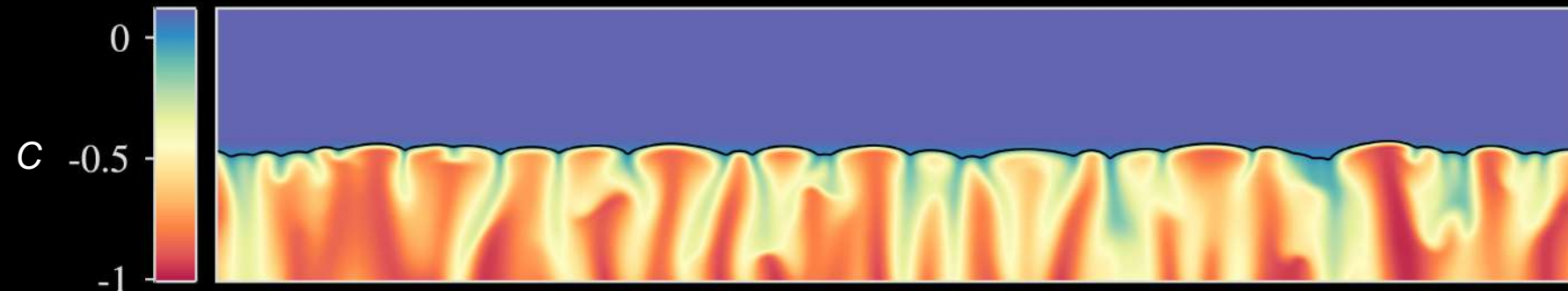
De Paoli & Pirozzoli  
(arXiv:2604.23199)



preprint



data



$\alpha = 0.1$   
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Theoretical framework for comparison of system with different b.c. and fluid models

Understanding and modelling of mixing dynamics

Comparison of different models and prediction of uncertainties/differences

De Paoli & Pirozzoli  
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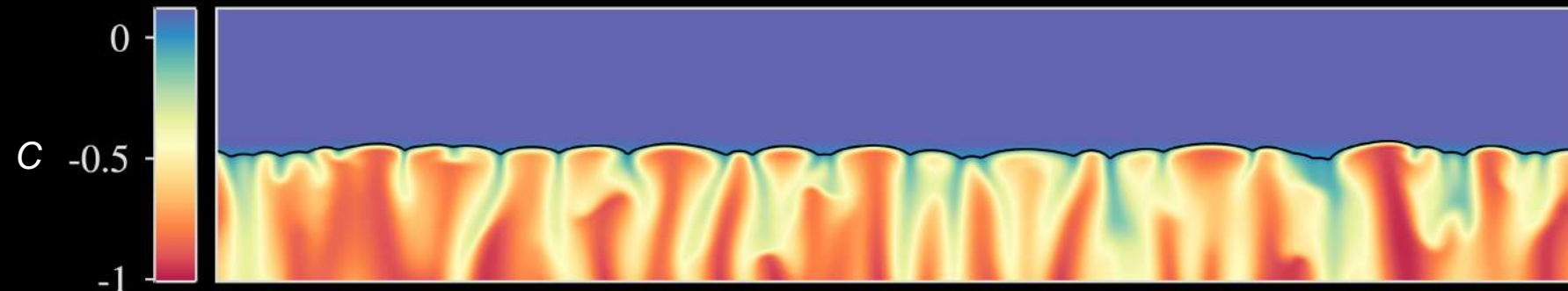


preprint



data

$\alpha = 0.1$   
 $\beta = 1.5$



Theoretical framework for comparison of system with different b.c. and fluid models

Understanding and modelling of mixing dynamics

Comparison of different models and prediction of uncertainties/differences



Funded by the European Union



European Research Council  
Established by the European Commission



Funded by the European Union (ERC, MORPHOS, 101163625). Views and opinions expressed are however those of the author(s) only and do not necessarily reflect those of the European Union or the European Research Council. Neither the European Union nor the granting authority can be held responsible for them. The results presented have been achieved using in part the Vienna Scientific Cluster (VSC).

De Paoli & Pirozzoli  
(arXiv:2604.23199)

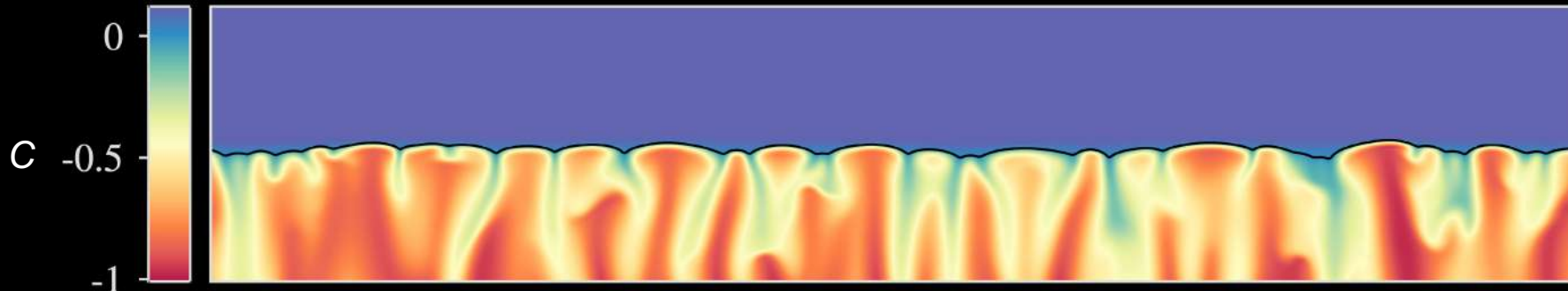


preprint



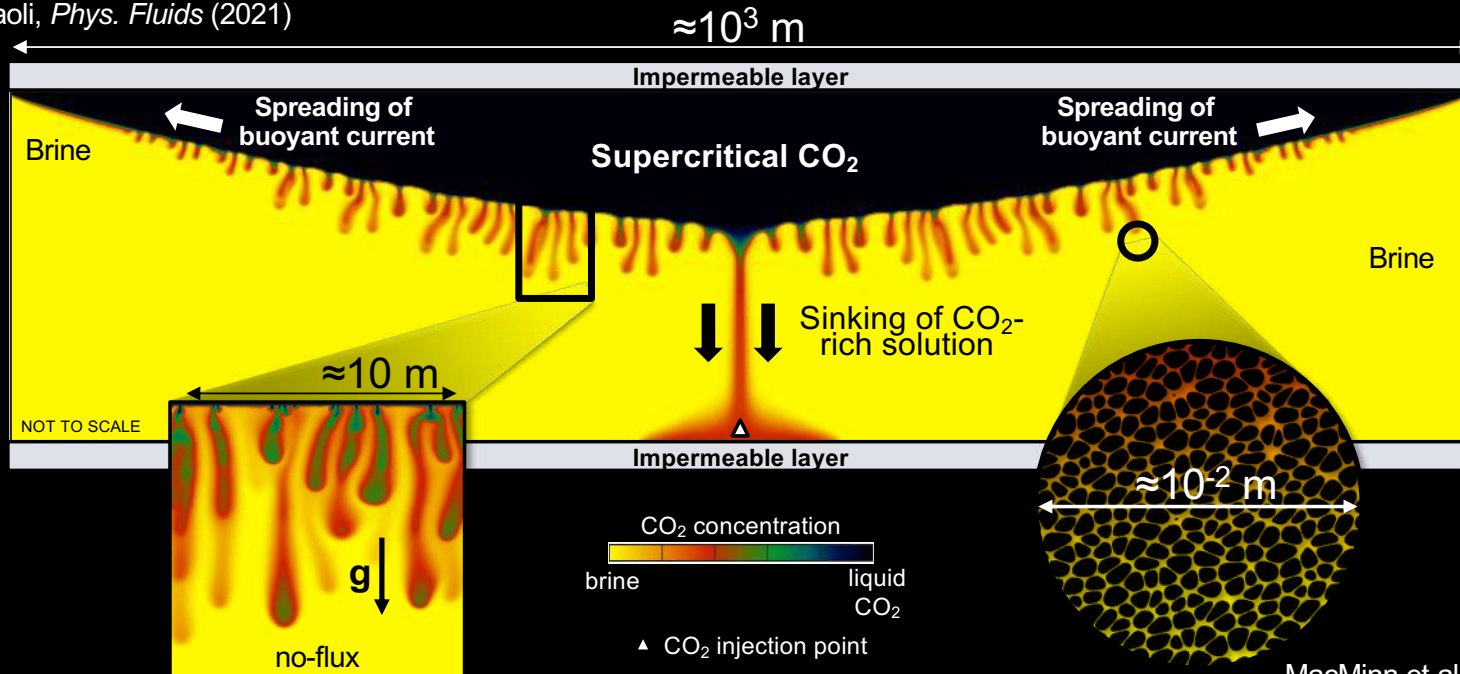
data

$\alpha = 0.1$   
 $\beta = 1.5$

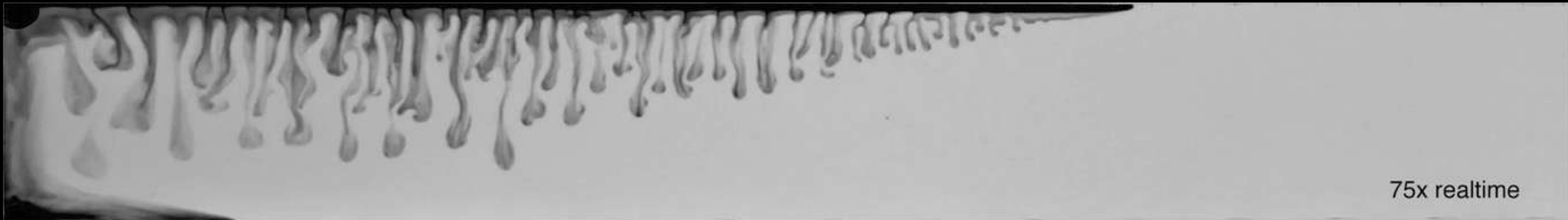




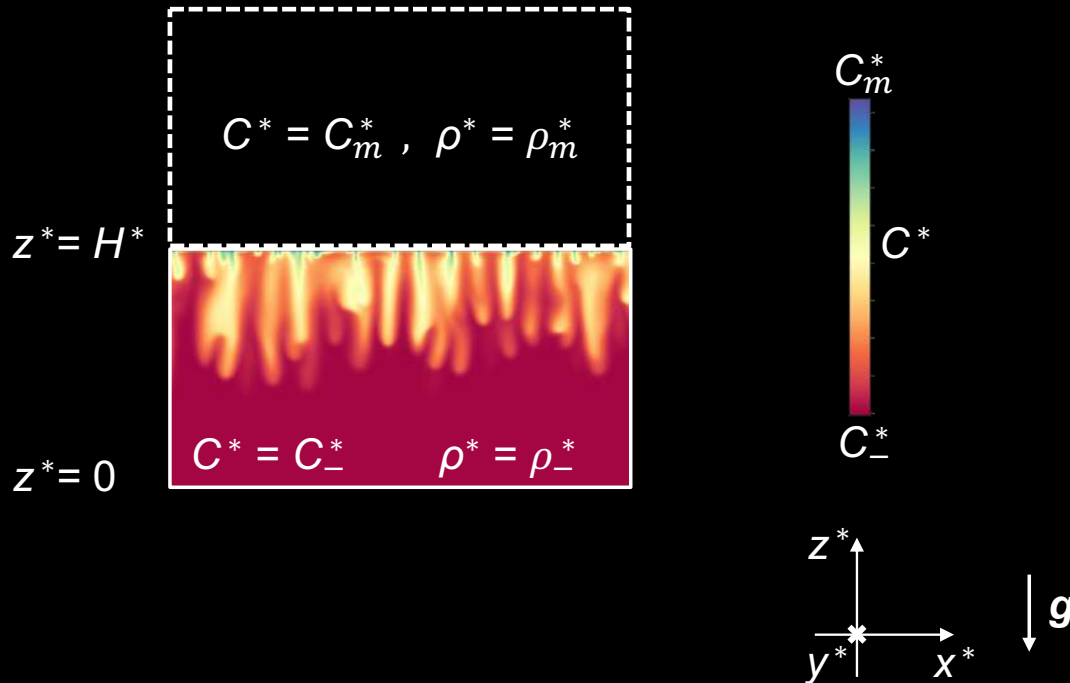
De Paoli, *Phys. Fluids* (2021)



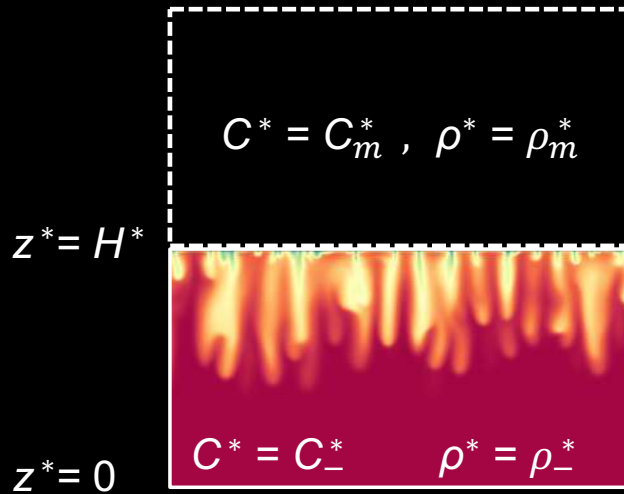
MacMinn et al., *Geophys. Res. Lett.* (2013)



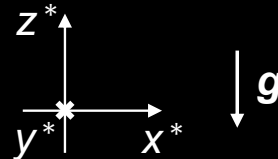
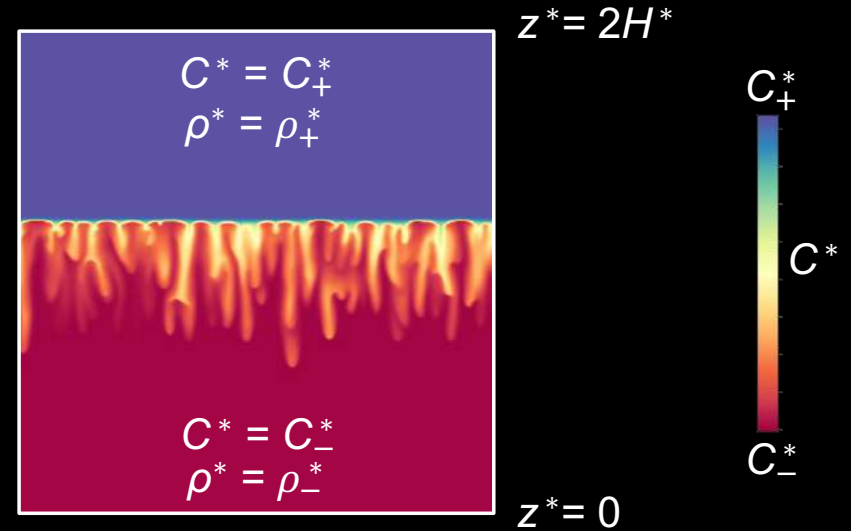
(a) fixed interface



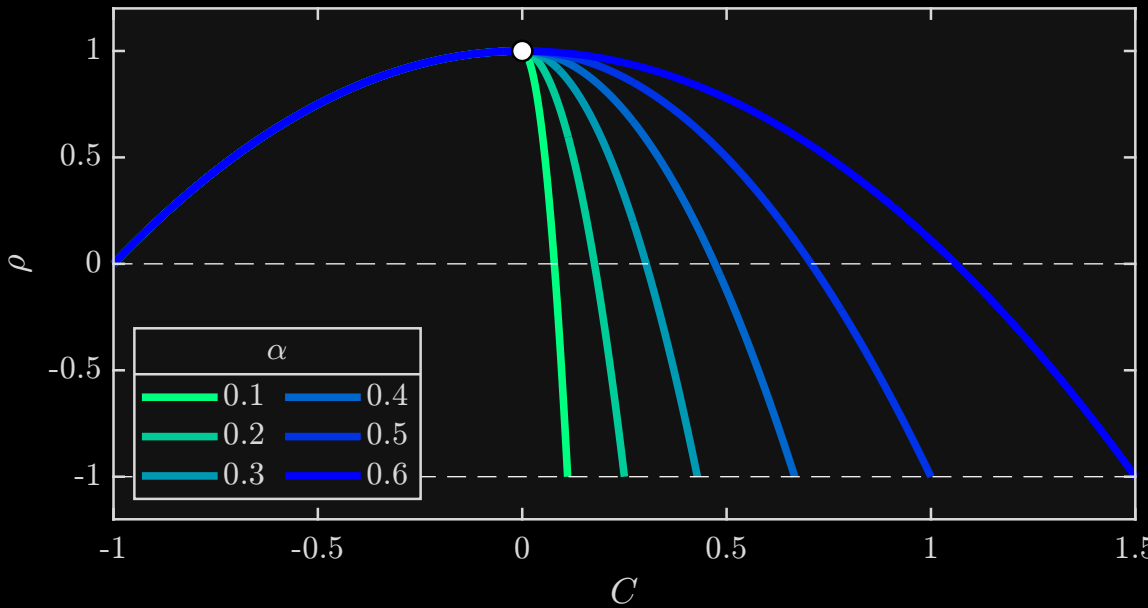
(a) fixed interface



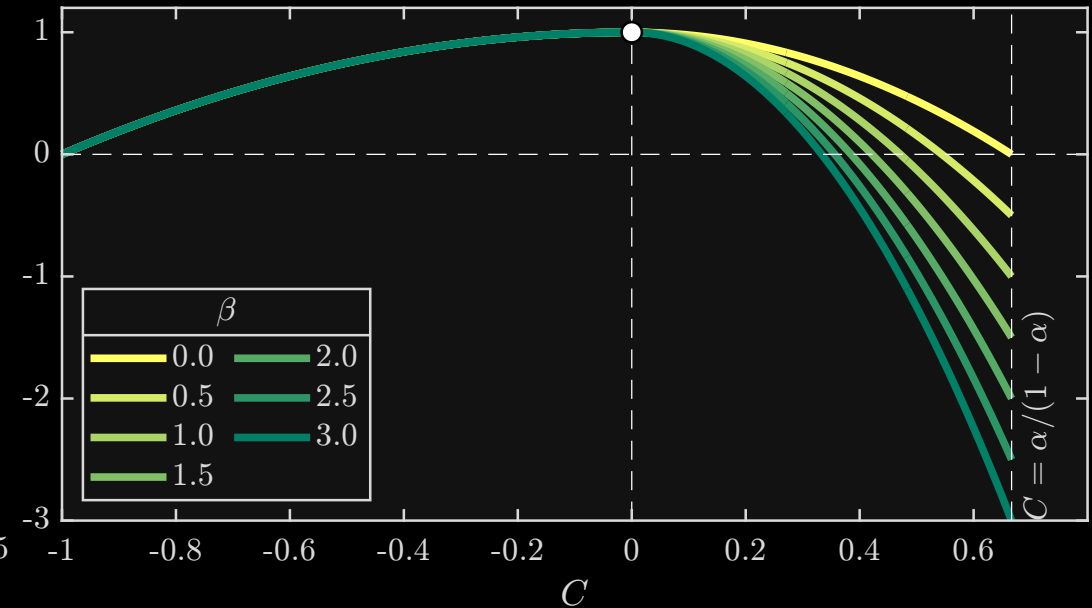
(b) free interface



### Effect of $\alpha$



### Effect of $\beta$



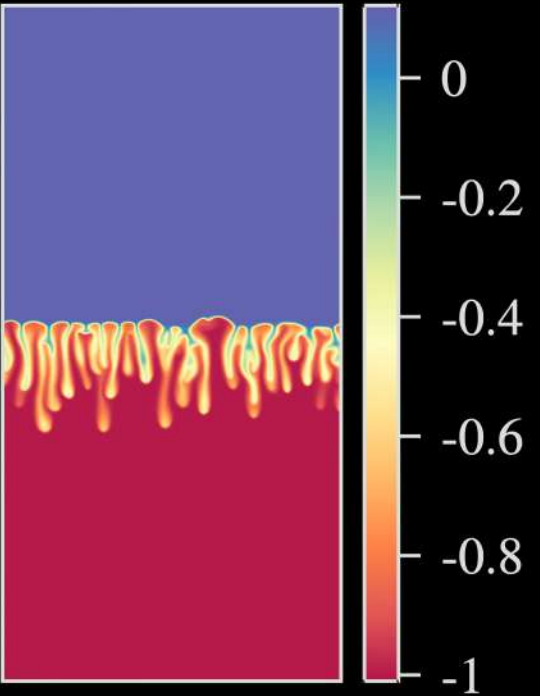
$$Ra_0 = \frac{\mathcal{U}^* H^*}{\phi D} \quad , \quad \alpha = \frac{C_+^* - C_m^*}{C_+^* - C_-^*} \quad , \quad \beta = \frac{\rho_-^* - \rho_+^*}{\rho_m^* - \rho_-^*}$$

*In this work*  
 $Ra_0 = 10^4$

$\alpha = 0.1, \beta = 0.0$

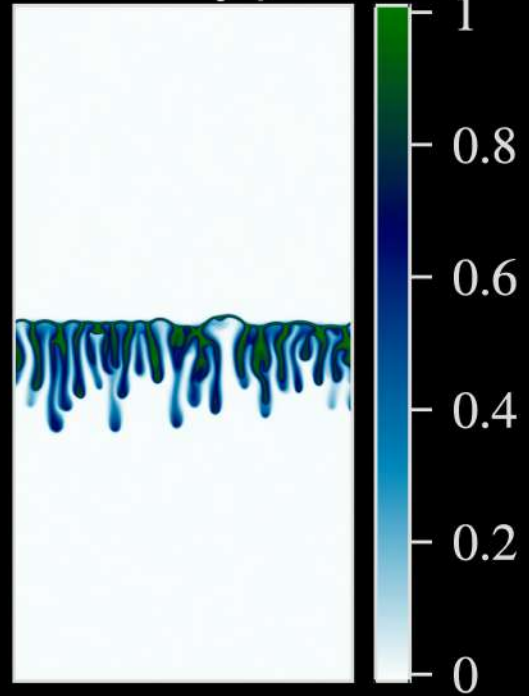
$t = 1.0$

concentration  $C$

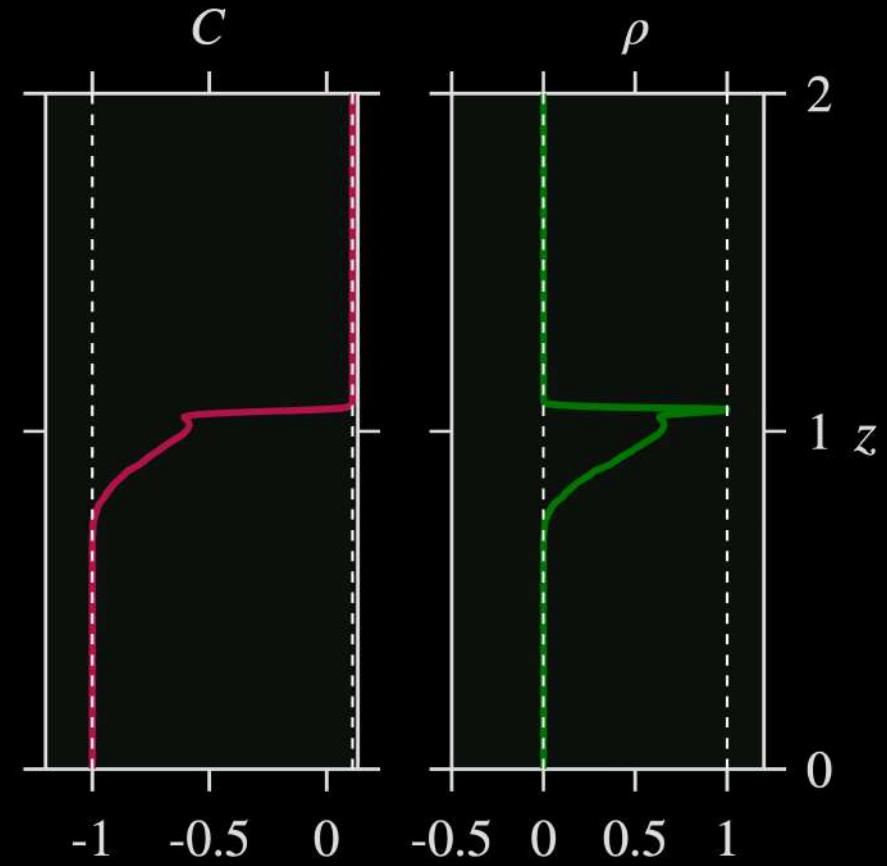


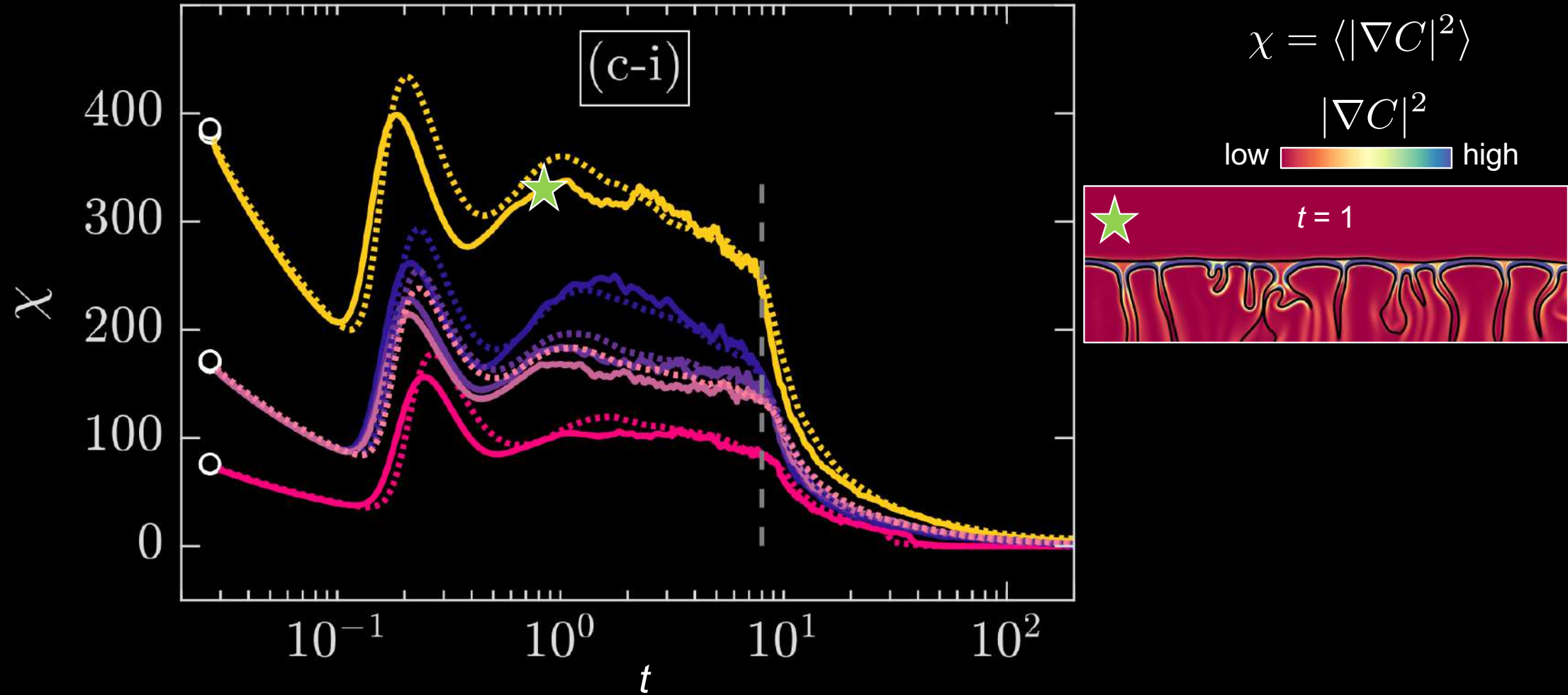
$C_{max} = 0.1$

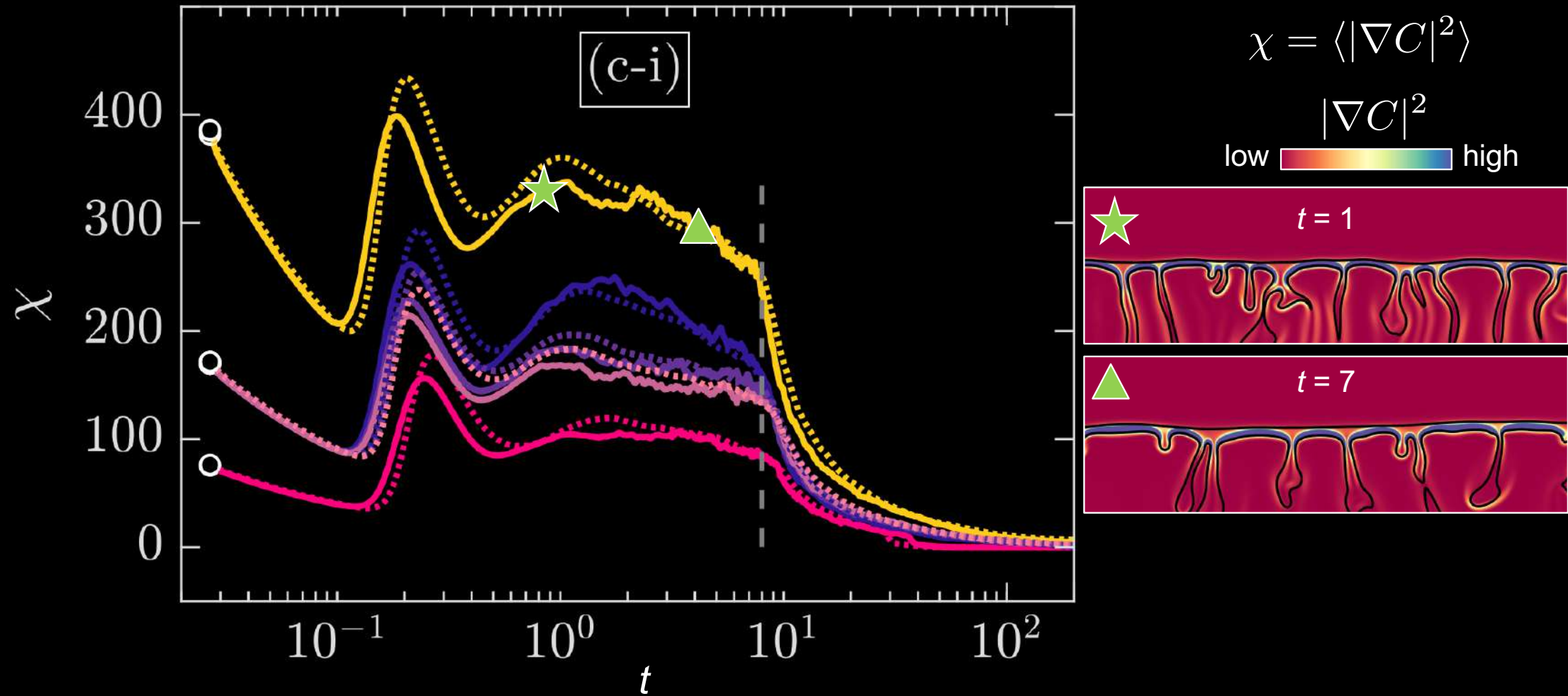
density  $\rho$

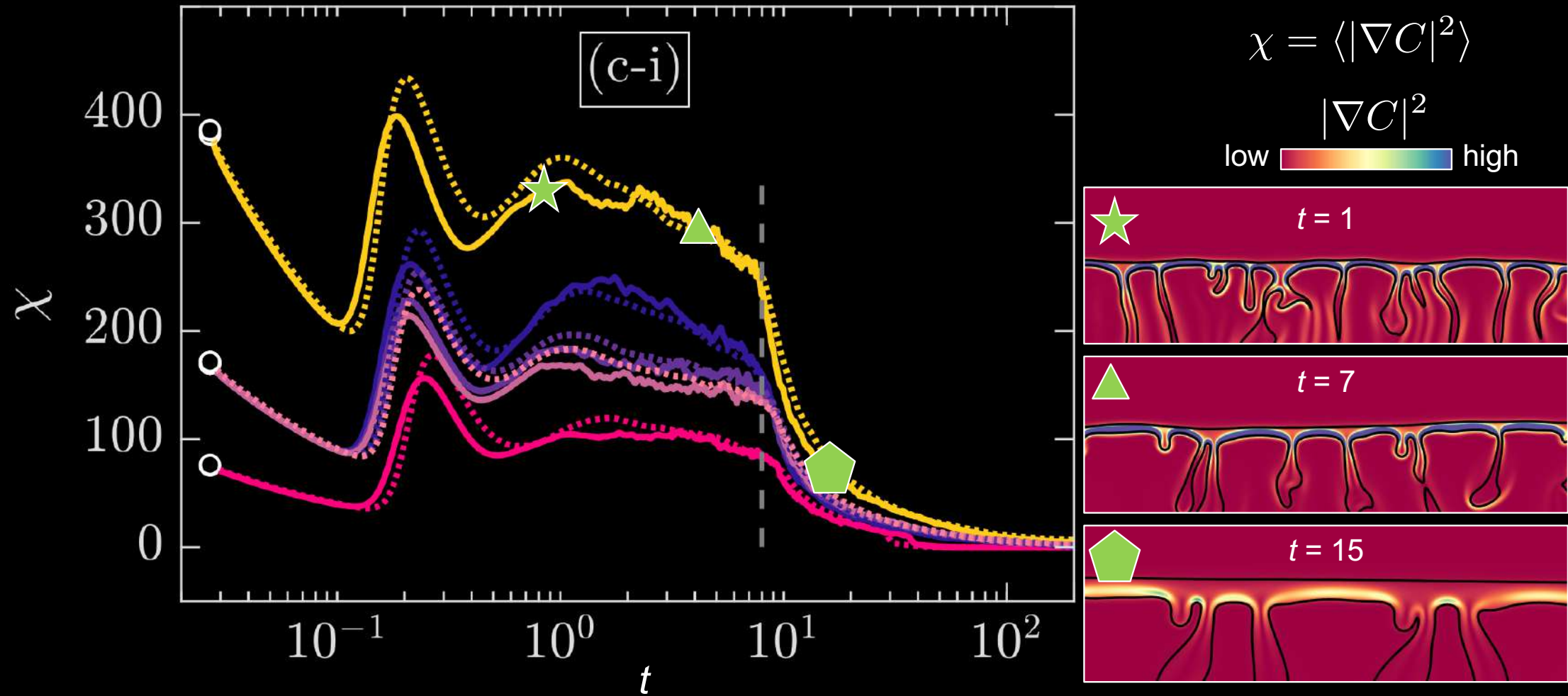


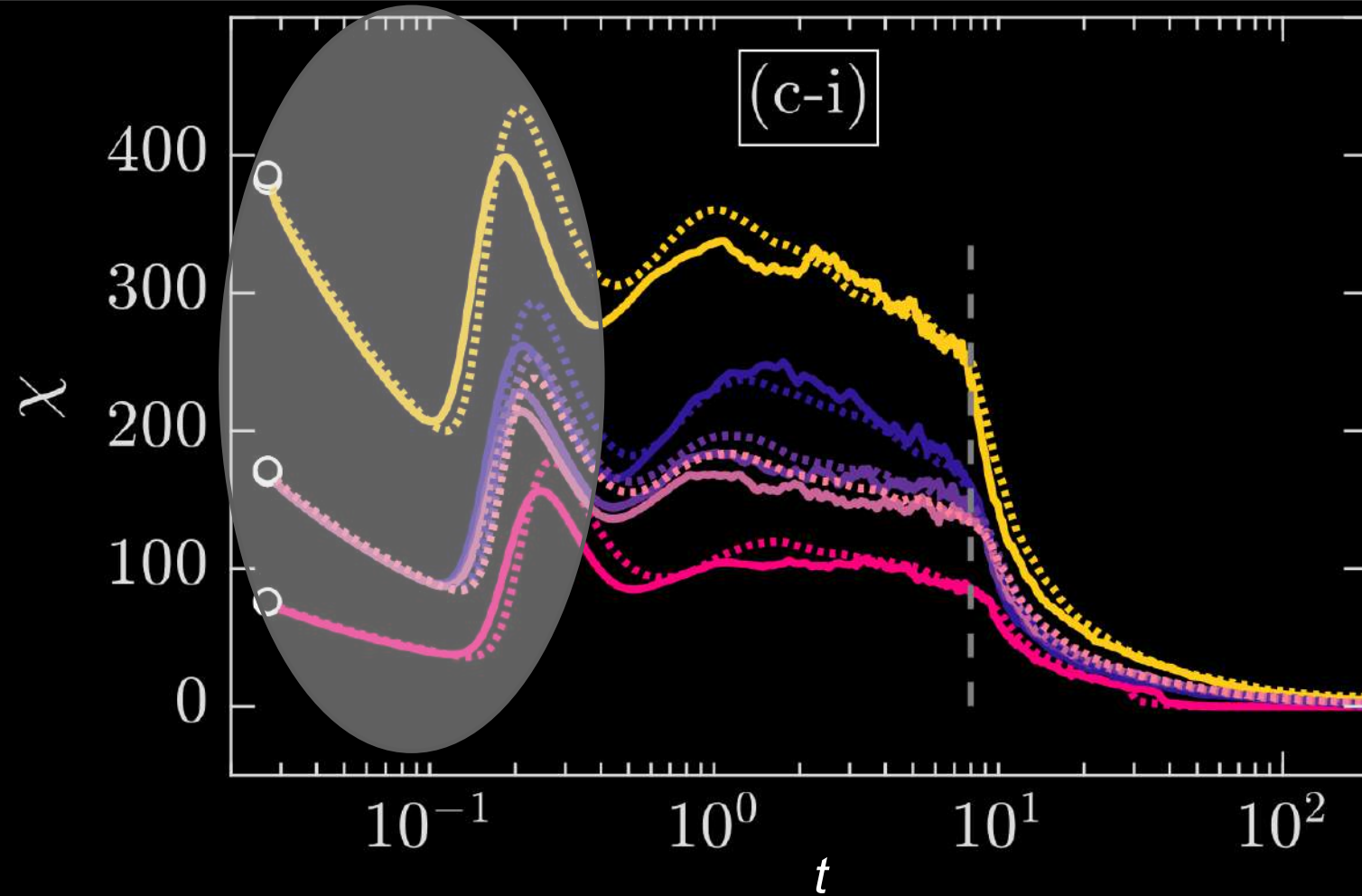
$\rho_{min} = -0.0$



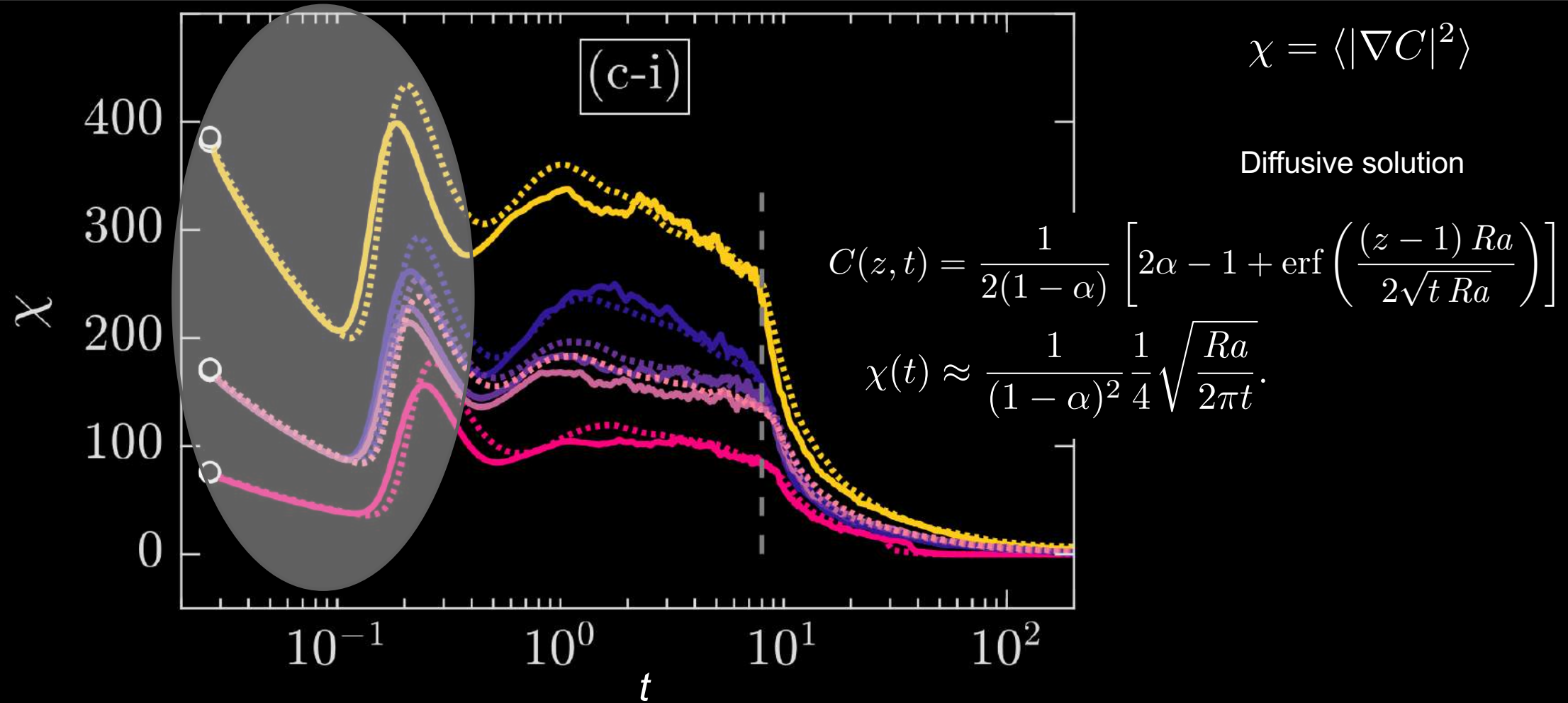


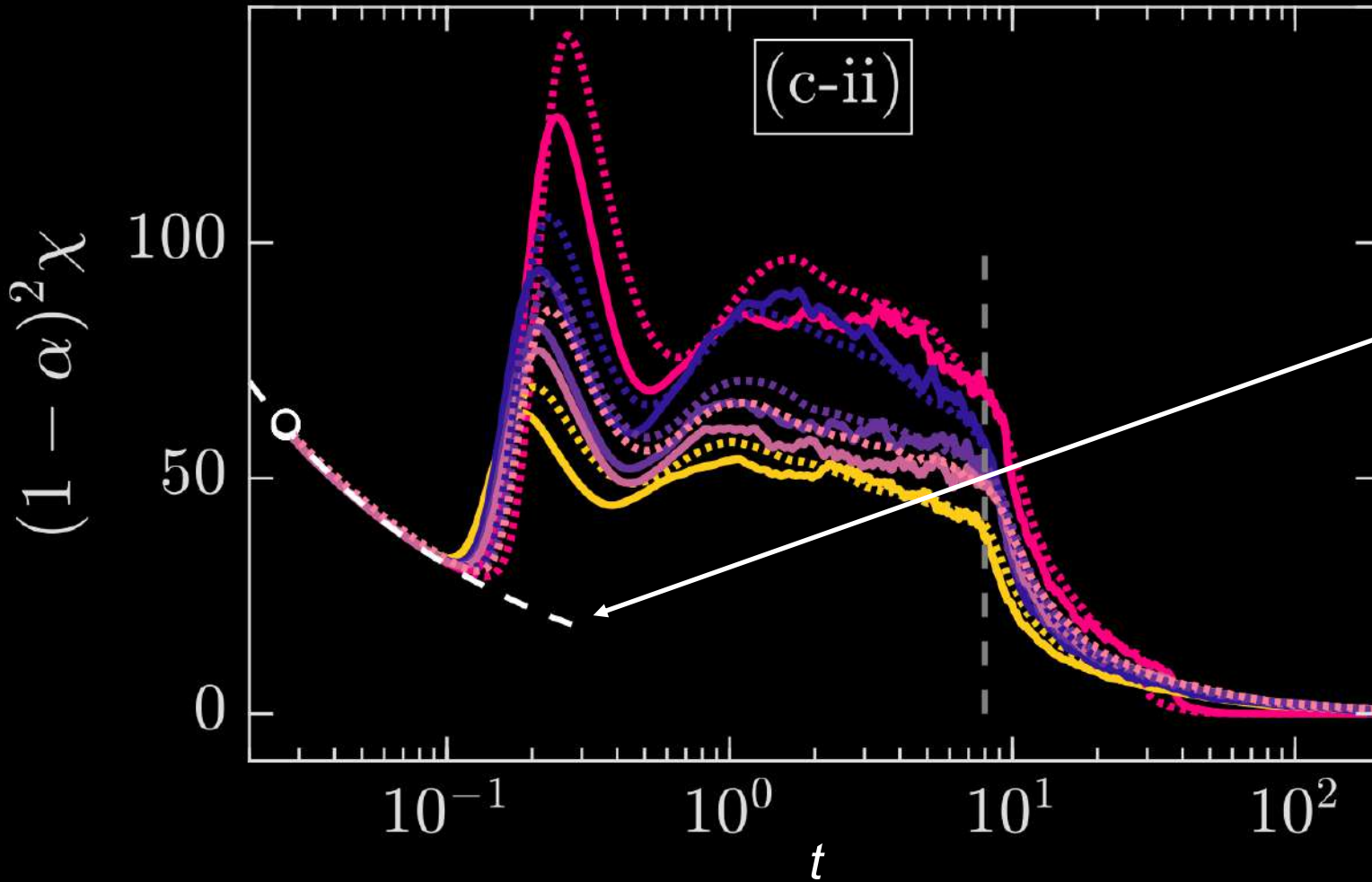




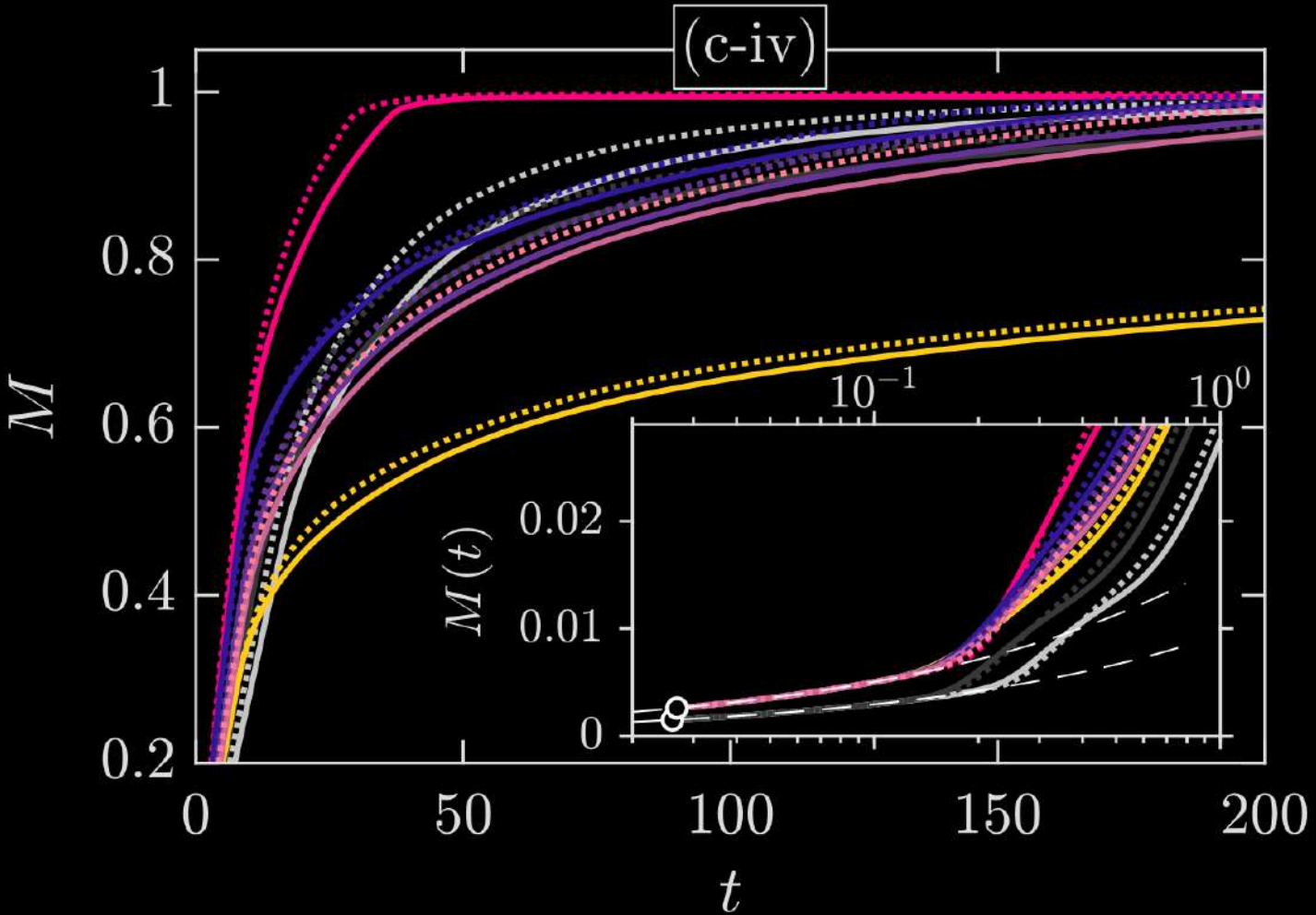


$$\chi = \langle |\nabla C|^2 \rangle$$





$$\chi(t) \approx \frac{1}{(1-\alpha)^2} \frac{1}{4} \sqrt{\frac{Ra}{2\pi t}}$$



$$M(t) = \frac{8(1 - \alpha)^2}{Ra} \int_0^t \chi dt$$

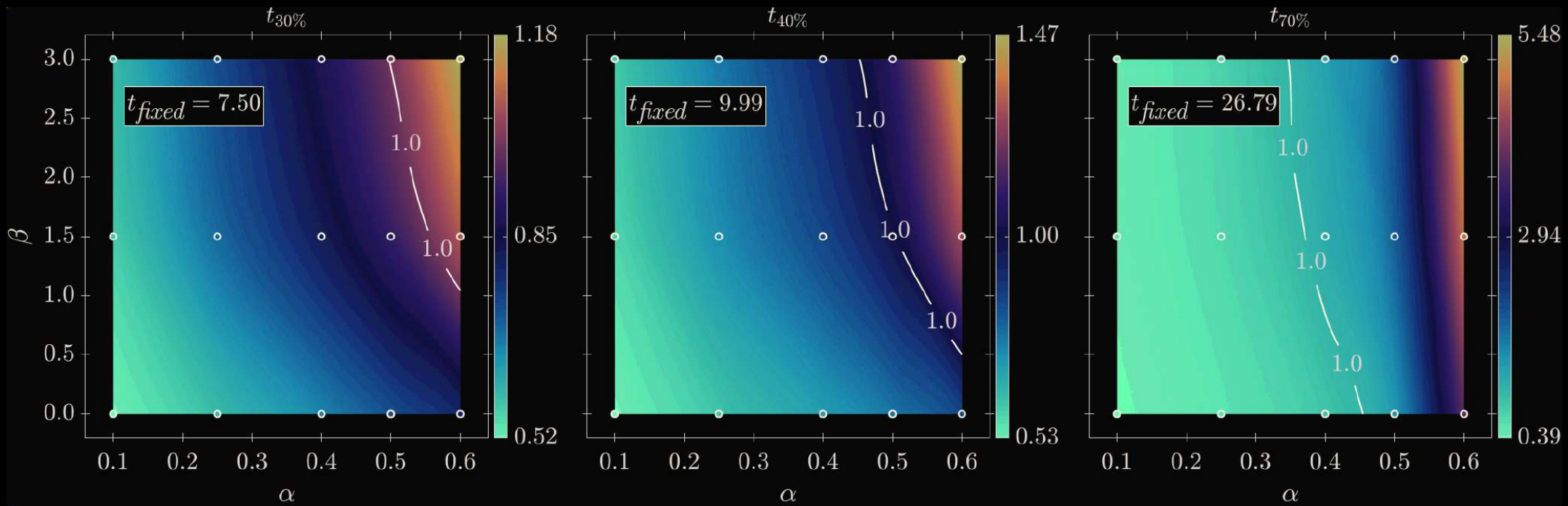
**fixed interface**

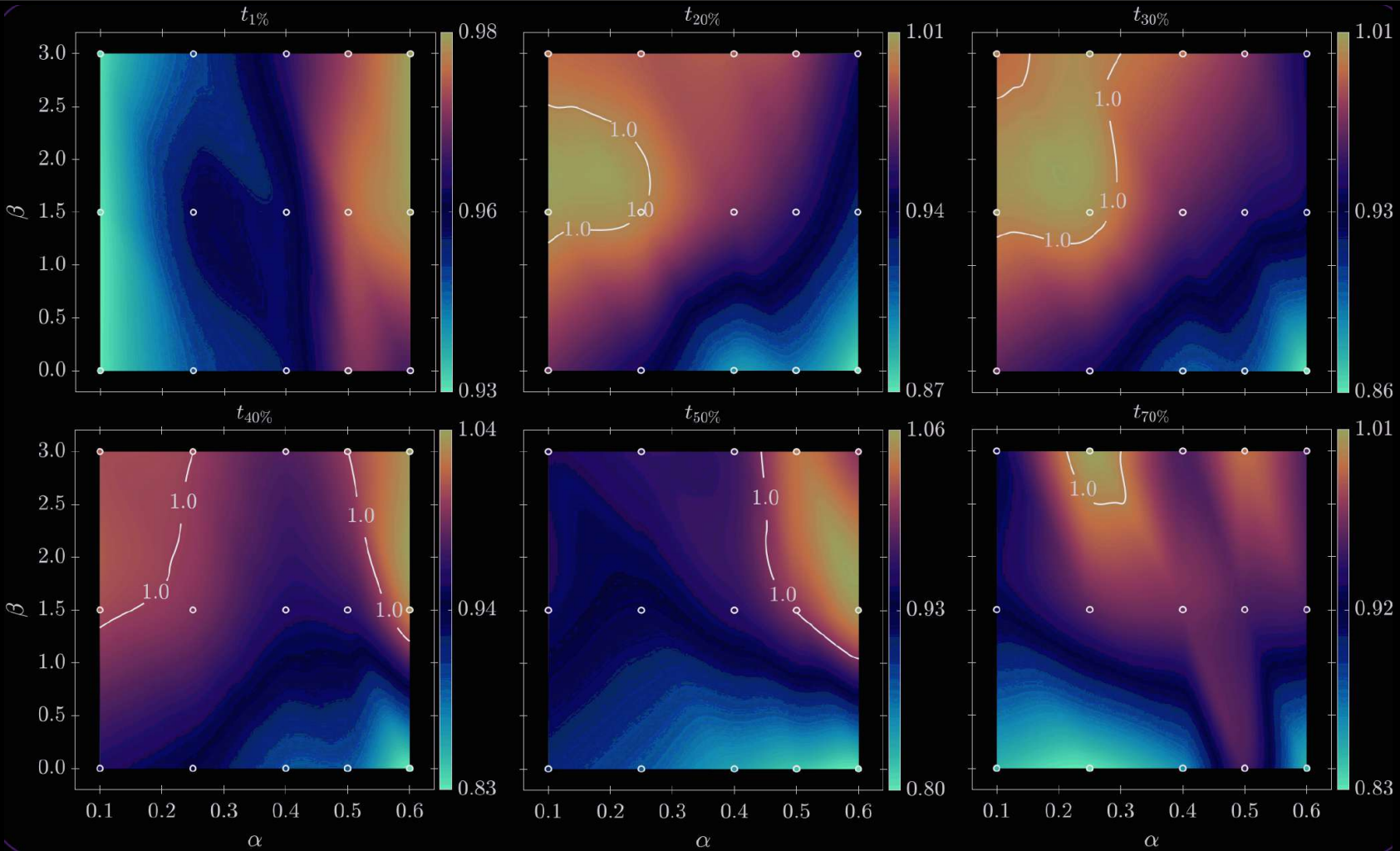
- A1 (2D)      ..... A3 (3D)
- A2 (2D)      ..... A4 (3D)

**free interface**

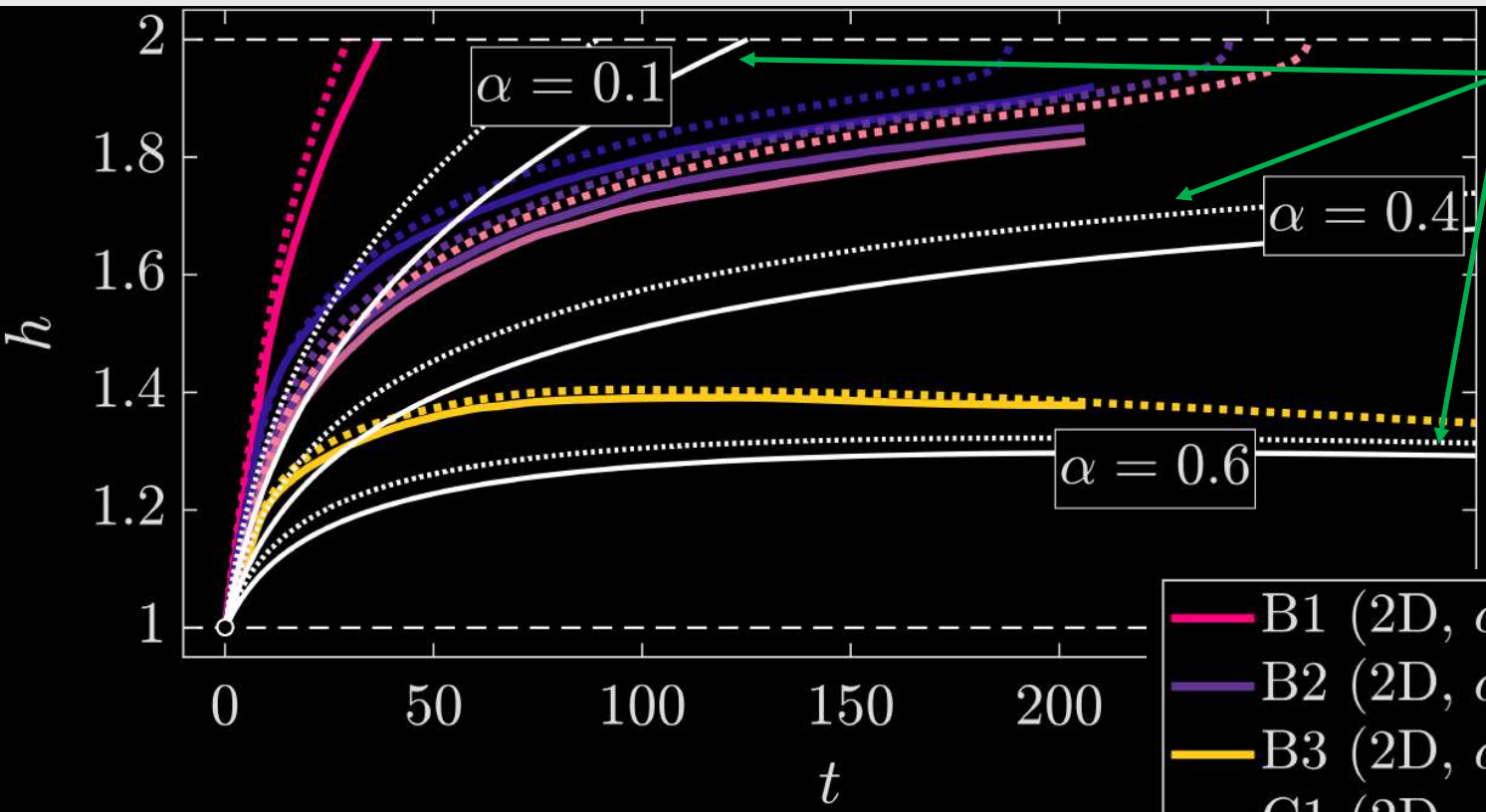
- B1 (2D)      ..... B4 (3D)
- B2 (2D)      ..... B5 (3D)
- B3 (2D)      ..... B6 (3D)
- C1 (2D)      ..... C4 (3D)
- C2 (2D)      ..... C5 (3D)
- C3 (2D)      ..... C6 (3D)

## $t_{\text{free}} / t_{\text{fixed}}$ (3D, parabolic)





$t_{2D} / t_{3D}$   
(free interface)



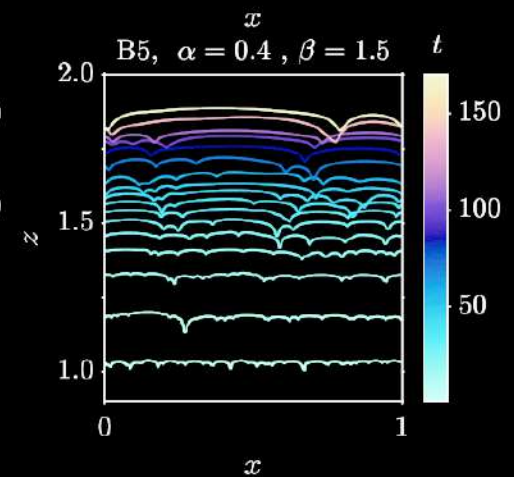
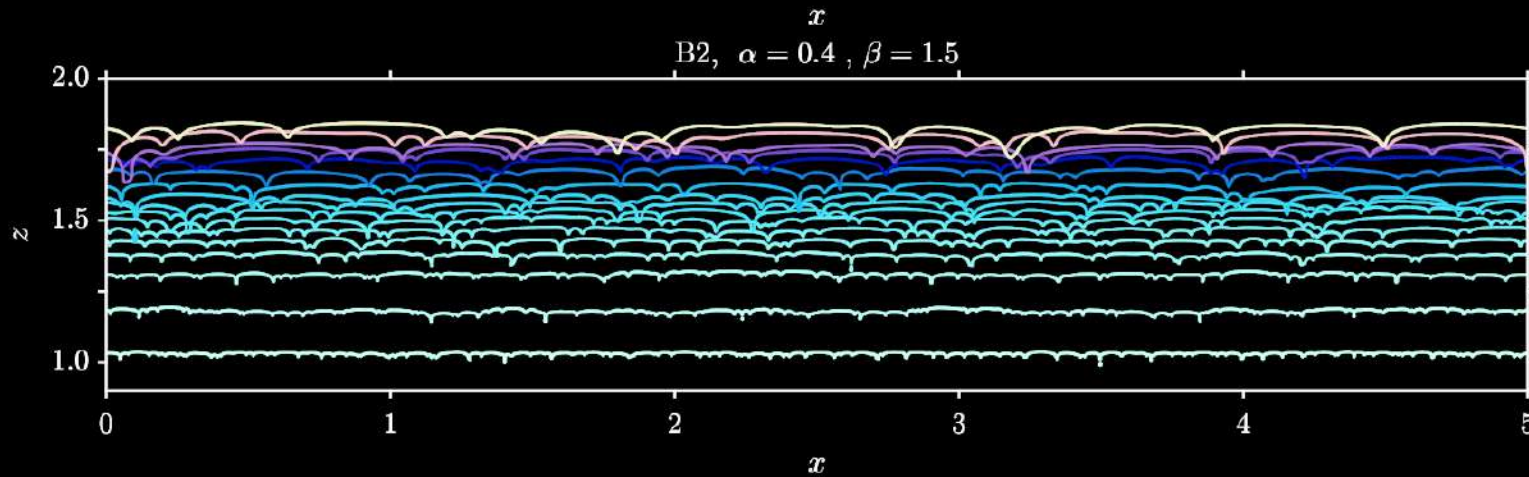
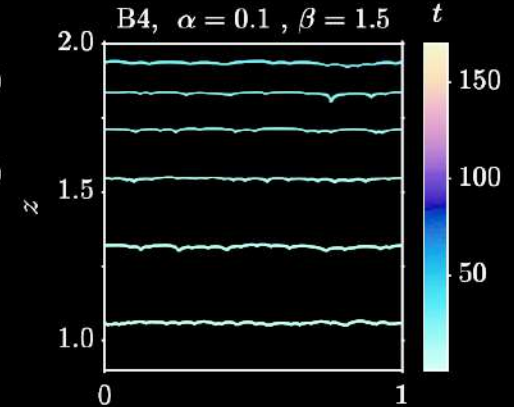
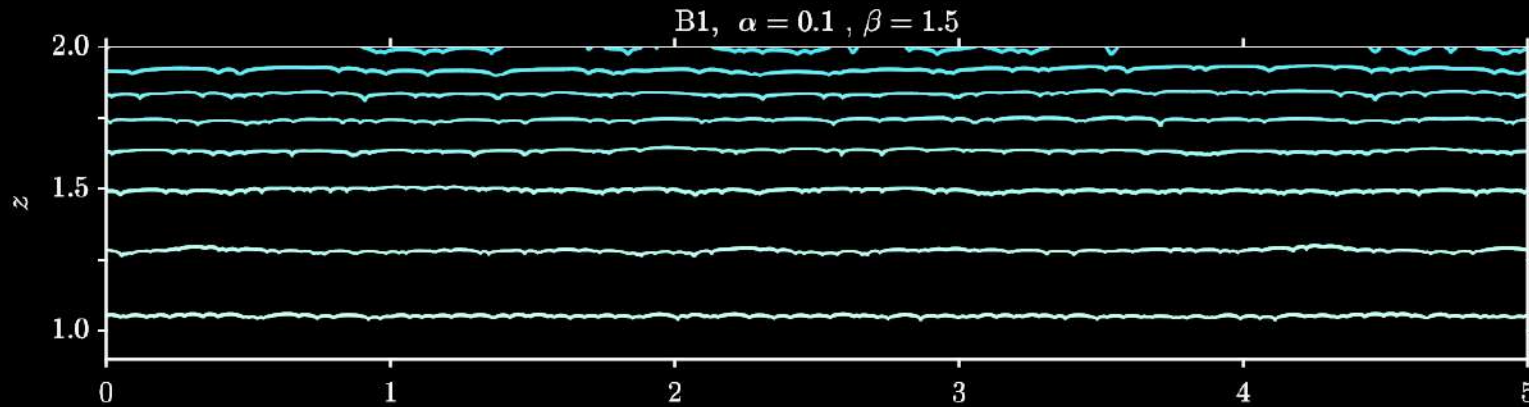
Model of Hewitt et al. (2013)

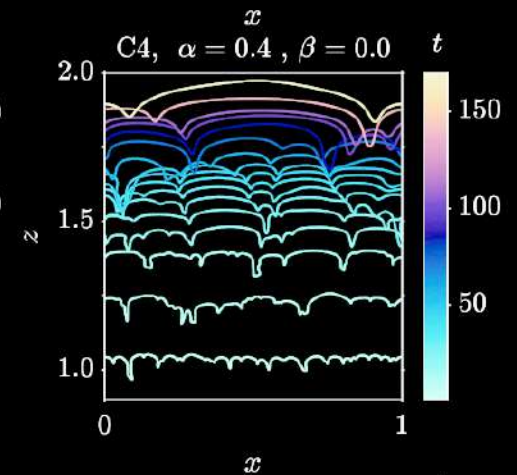
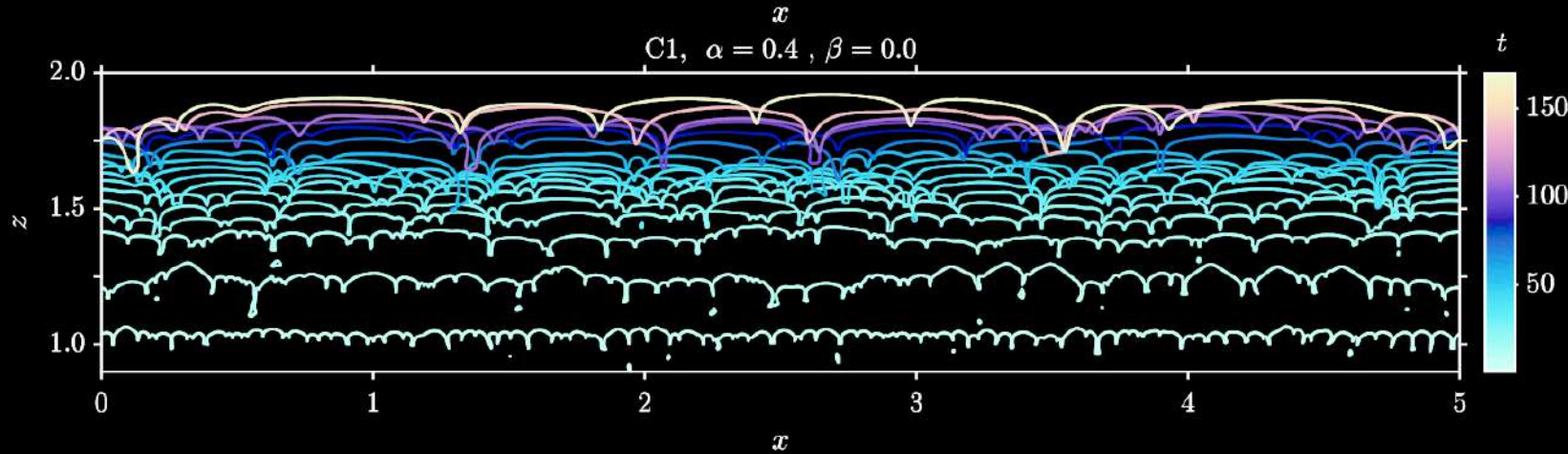
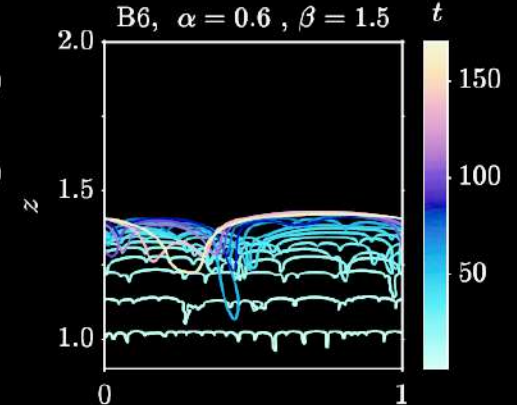
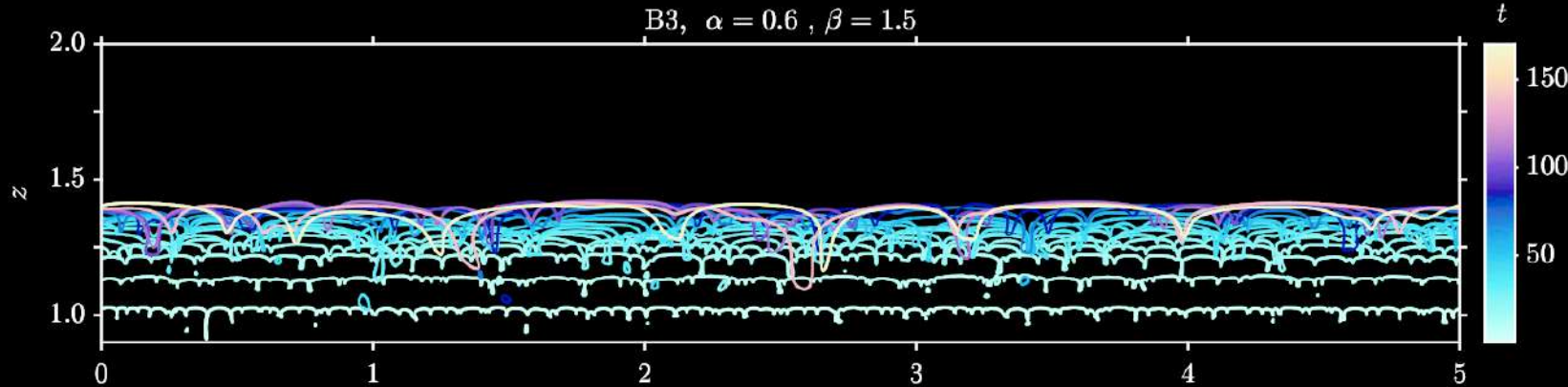
$$h \frac{d\Theta}{dt} = \frac{|\Theta|}{h Ra} Nu_e$$

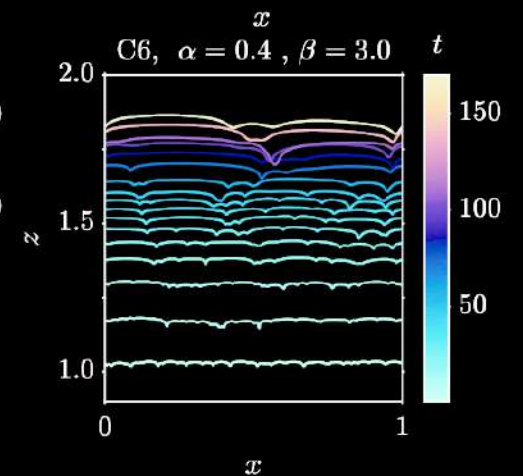
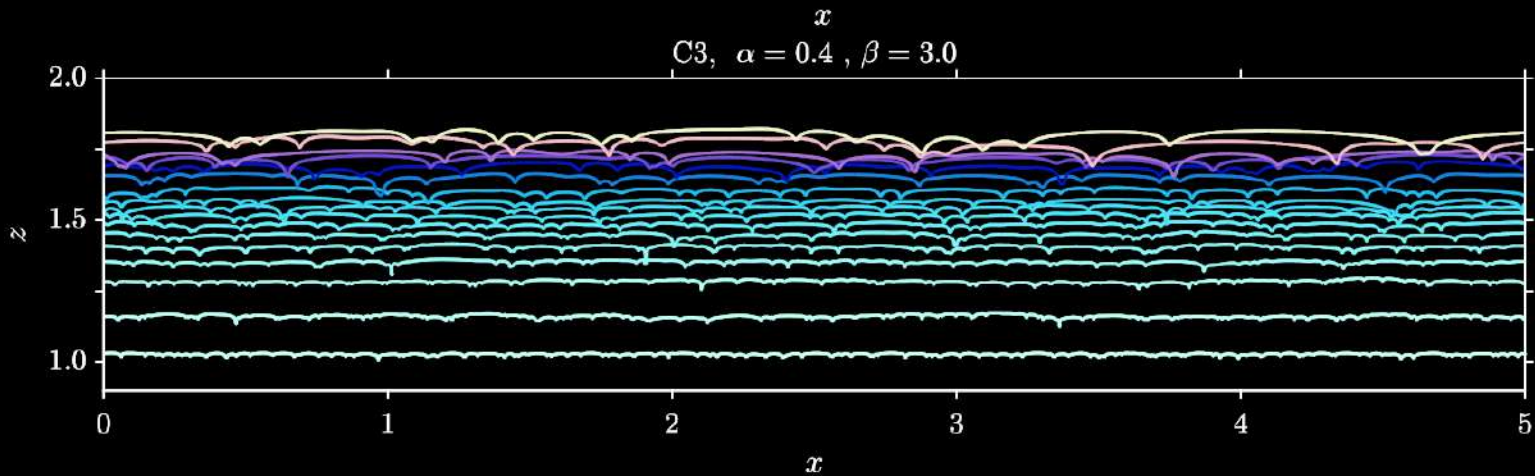
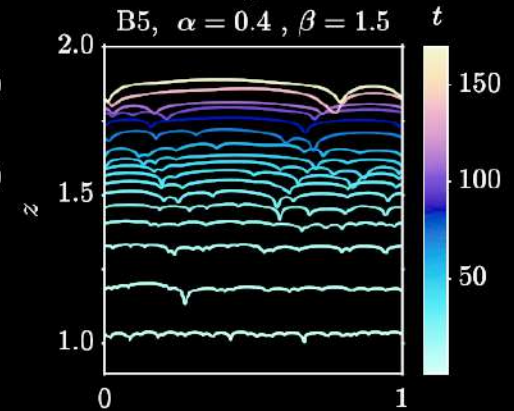
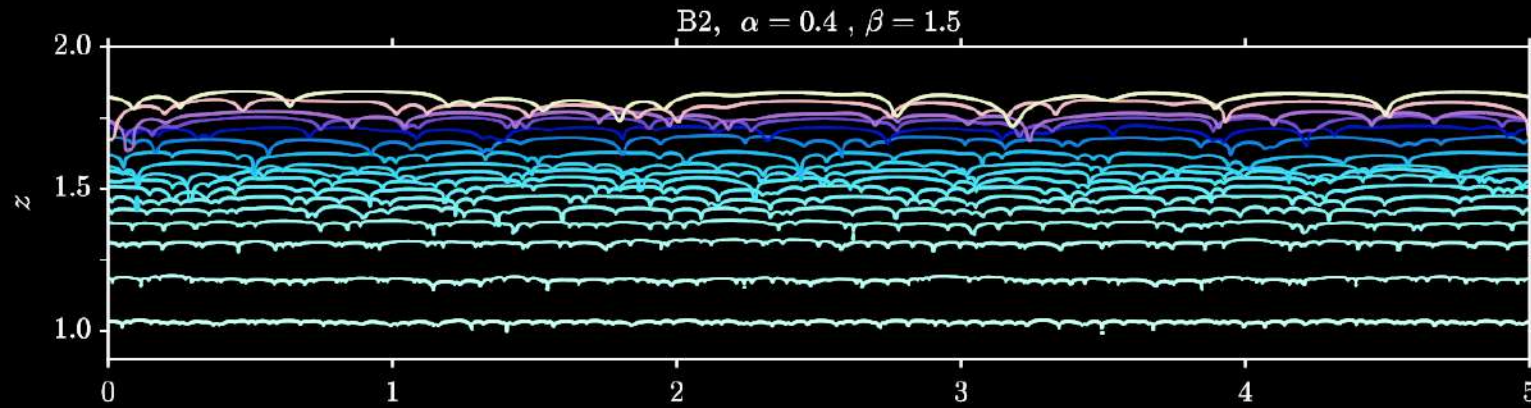
$$\left( |\Theta| + C_+ - \frac{2C_+}{\pi} \right) \frac{dh}{dt} = -\frac{4C_+}{\pi \delta Ra} + \frac{|\Theta| Nu_e}{h Ra}$$

$$\left( |\Theta| + C_+ - \frac{2C_+}{\pi} \right) \frac{d\delta}{dt} = \frac{8(C_+ + \Theta)}{\pi \delta Ra} - \frac{4|\Theta| Nu_e}{\pi h Ra}$$

- |                            |                            |
|----------------------------|----------------------------|
| — B1 (2D, $\alpha = 0.1$ ) | ⋯ B4 (3D, $\alpha = 0.1$ ) |
| — B2 (2D, $\alpha = 0.4$ ) | ⋯ B5 (3D, $\alpha = 0.4$ ) |
| — B3 (2D, $\alpha = 0.6$ ) | ⋯ B6 (3D, $\alpha = 0.6$ ) |
| — C1 (2D, $\alpha = 0.4$ ) | ⋯ C4 (3D, $\alpha = 0.4$ ) |
| — C2 (2D, $\alpha = 0.4$ ) | ⋯ C5 (3D, $\alpha = 0.4$ ) |
| — C3 (2D, $\alpha = 0.4$ ) | ⋯ C6 (3D, $\alpha = 0.4$ ) |







Sim.	interface/b.c.	$Ra$	$\rho(C)$	$\alpha$	$\beta$	$L_x$	$L_y$	$L_z$	$N_x$	$N_y$	$N_z$
A1	fixed/(8)	$1 \times 10^4$	linear (S6)	-	-	5	-	1	5120	1	256
A2	fixed/(8)	$1 \times 10^4$	parabolic (S7)	-	-	5	-	1	5120	1	256
A3	fixed/(8)	$1 \times 10^4$	linear (S6)	-	-	1	1	1	1024	1024	256
A4	fixed/(8)	$1 \times 10^4$	parabolic (S7)	-	-	1	1	1	1024	1024	256
B1	free/(9)	$1 \times 10^4$	piecewise (S8)	0.1	1.5	5	-	2	5120	1	1024
B2≡C2	free/(9)	$1 \times 10^4$	piecewise (S8)	0.4	1.5	5	-	2	5120	1	1024
B3	free/(9)	$1 \times 10^4$	piecewise (S8)	0.6	1.5	5	-	2	5120	1	1024
B4	free/(9)	$1 \times 10^4$	piecewise (S8)	0.1	1.5	1	1	2	1024	1024	1024
B5≡C5	free/(9)	$1 \times 10^4$	piecewise (S8)	0.4	1.5	1	1	2	1024	1024	1024
B6	free/(9)	$1 \times 10^4$	piecewise (S8)	0.6	1.5	1	1	2	1024	1024	1024
C1	free/(9)	$1 \times 10^4$	piecewise (S8)	0.4	0.0	5	-	2	5120	1	1024
C2≡B2	free/(9)	$1 \times 10^4$	piecewise (S8)	0.4	1.5	5	-	2	5120	1	1024
C3	free/(9)	$1 \times 10^4$	piecewise (S8)	0.4	3.0	5	-	2	5120	1	1024
C4	free/(9)	$1 \times 10^4$	piecewise (S8)	0.4	0.0	1	1	2	1024	1024	1024
C5≡B5	free/(9)	$1 \times 10^4$	piecewise (S8)	0.4	1.5	1	1	2	1024	1024	1024
C6	free/(9)	$1 \times 10^4$	piecewise (S8)	0.4	3.0	1	1	2	1024	1024	1024

Sim.	interface/b.c.	$Ra$	$\rho(C)$	$\alpha$	$\beta$	$L_x$	$L_y$	$L_z$	$N_x$	$N_y$	$N_z$
D1	free/(9)	$1 \times 10^4$	piecewise (S8)	0.25	0.0	5	-	2	5120	1	1024
D2	free/(9)	$1 \times 10^4$	piecewise (S8)	0.25	1.5	5	-	2	5120	1	1024
D3	free/(9)	$1 \times 10^4$	piecewise (S8)	0.25	3.0	5	-	2	5120	1	1024
D4	free/(9)	$1 \times 10^4$	piecewise (S8)	0.5	0.0	5	-	2	5120	1	1024
D5	free/(9)	$1 \times 10^4$	piecewise (S8)	0.5	1.5	5	-	2	5120	1	1024
D6	free/(9)	$1 \times 10^4$	piecewise (S8)	0.5	3.0	5	-	2	5120	1	1024
D7	free/(9)	$1 \times 10^4$	piecewise (S8)	0.25	0.0	1	1	2	1024	1024	1024
D8	free/(9)	$1 \times 10^4$	piecewise (S8)	0.25	1.5	1	1	2	1024	1024	1024
D9	free/(9)	$1 \times 10^4$	piecewise (S8)	0.25	3.0	1	1	2	1024	1024	1024
D10	free/(9)	$1 \times 10^4$	piecewise (S8)	0.5	0.0	1	1	2	1024	1024	1024
D11	free/(9)	$1 \times 10^4$	piecewise (S8)	0.5	1.5	1	1	2	1024	1024	1024
D12	free/(9)	$1 \times 10^4$	piecewise (S8)	0.5	3.0	1	1	2	1024	1024	1024
E1	free/(9)	$1 \times 10^4$	piecewise (S8)	0.1	0.0	5	-	2	5120	1	1024
E2	free/(9)	$1 \times 10^4$	piecewise (S8)	0.6	0.0	5	-	2	5120	1	1024
E3	free/(9)	$1 \times 10^4$	piecewise (S8)	0.1	3.0	5	-	2	5120	1	1024
E4	free/(9)	$1 \times 10^4$	piecewise (S8)	0.6	3.0	5	-	2	5120	1	1024
E5	free/(9)	$1 \times 10^4$	piecewise (S8)	0.1	0.0	1	1	2	1024	1024	1024
E6	free/(9)	$1 \times 10^4$	piecewise (S8)	0.6	0.0	1	1	2	1024	1024	1024
E7	free/(9)	$1 \times 10^4$	piecewise (S8)	0.1	3.0	1	1	2	1024	1024	1024
E8	free/(9)	$1 \times 10^4$	piecewise (S8)	0.6	3.0	1	1	2	1024	1024	1024